

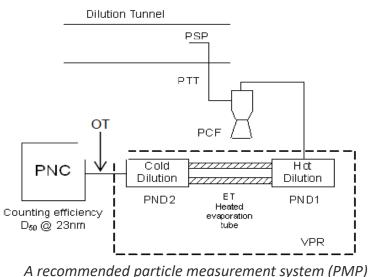
# An Ultrafine Particle Number Measurement System Operating Under Wide Temperature Range

Wide Temperature Condensation Particle Counter(WTCPC)

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2021.12.1

### **Background: Nanometer Particle Number (PN) Regulations**

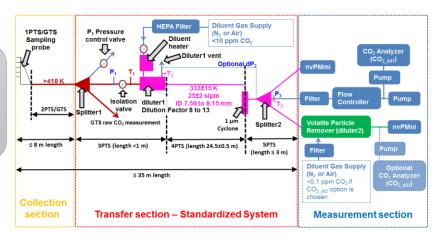
PN regulation for vehicles







PN regulation for aviation

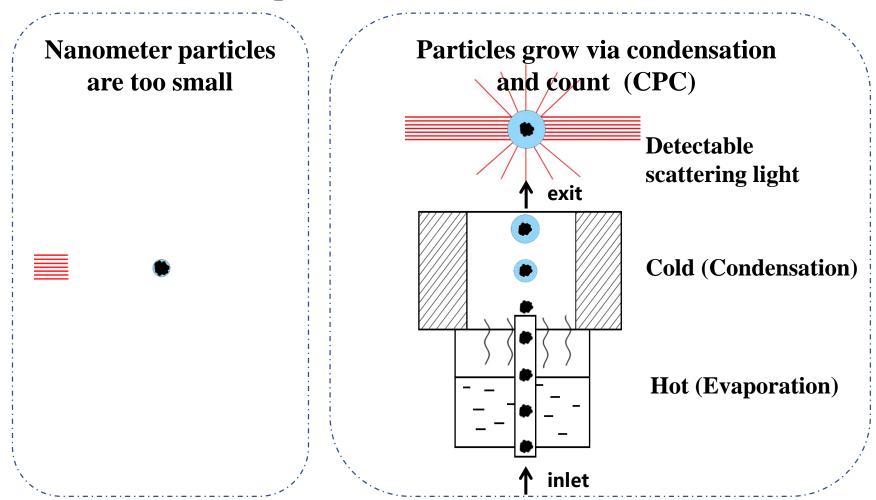


A recommended nvPM measurement system (SAE E31)



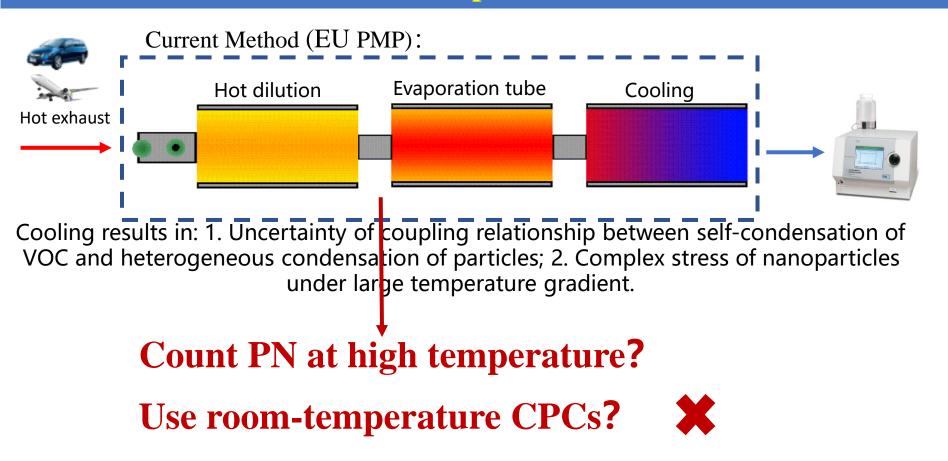
### **Condensation Particle Counter (CPC) is the only compliant method\***

Traditional techniques: filter-based, thermoacoustic, etc.



# Background: Traditional Method 'Uncertain'

Hot exhaust PN measurement: first cooling and then count PN using CPC. The measurement error is up to 40% (J.AerosolSci.,2011,42:883–897).



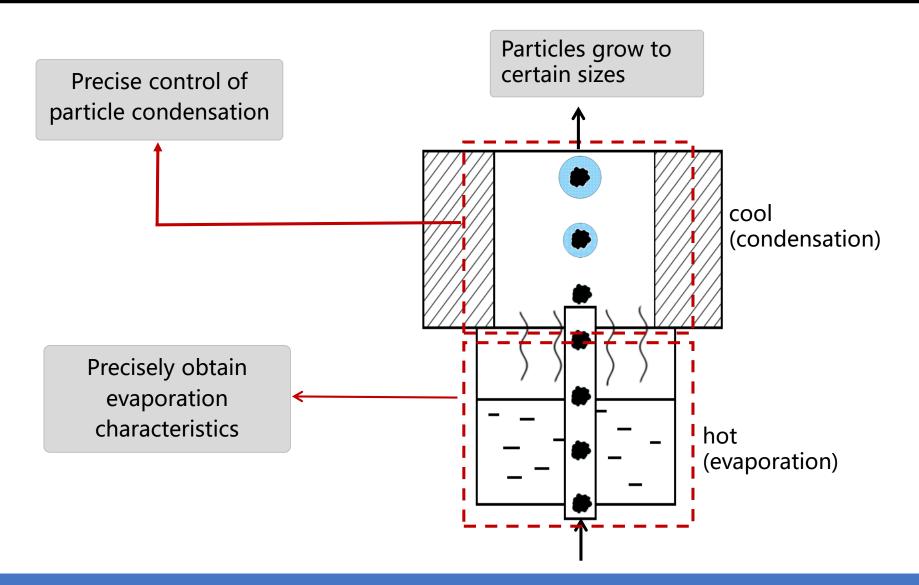
It is difficult to count PN after condensation at high temperature.

# Design new working liquid to realize wide temperature CPC

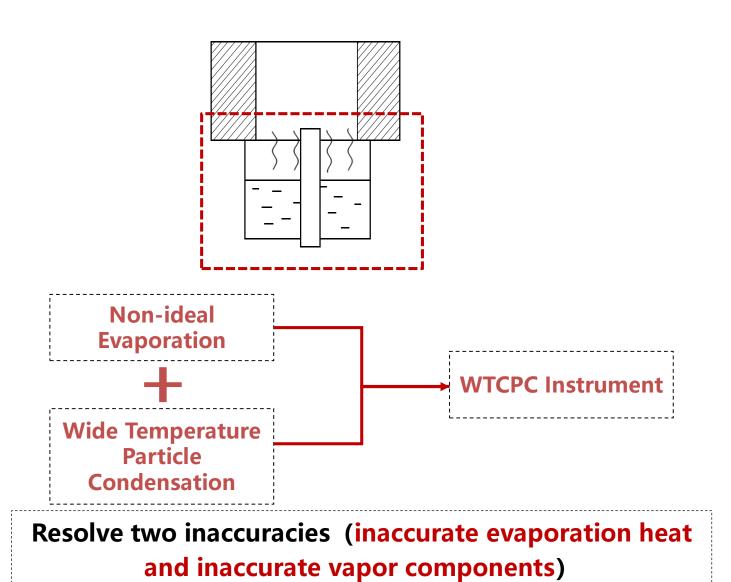
	Condensation working liquid	Working temperature
Amercian TSI 9001 CPC	water	<35°C
German Grimm 5400 CPC	N-butyl alcohol	<40°C
Amercian TSI 9310 CPC	Isopropyl alcohol	<40°C
Finland Airmodus A10 CPC	Diethylene glycol monoethyl ether	<45°C
Beihang WTCPC	Non-ideal liquid mixture	10200°C

All existing CPCs use pure substances while WTCPC adopts a strongly non-ideal mixture as condensation working liquid.

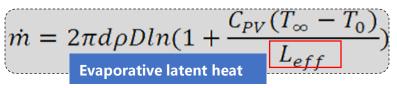
# Design new working liquid to realize wide temperature CPC



Challenge for predicting evaporation and condensation due to non-ideality.



# Prob. Low calculation accuracy of latent heat of evaporation







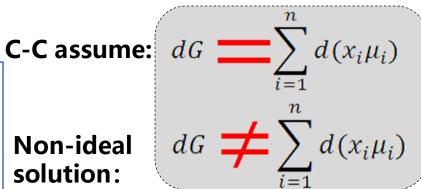


Non-ideal

**Equation Clausius-Clapeyron** 

# Inherent defect:

C-C equation ignores the chemical potential increase caused by mixture non-ideality.



# Difficuty

The chemical potential increase is difficult to calculate due to the lack of high temperature data

$$dG = \sum_{i=1}^{n} d(x_{i} \mu_{i}) + f(x_{i}, \theta_{m}, \Psi_{m,n})$$

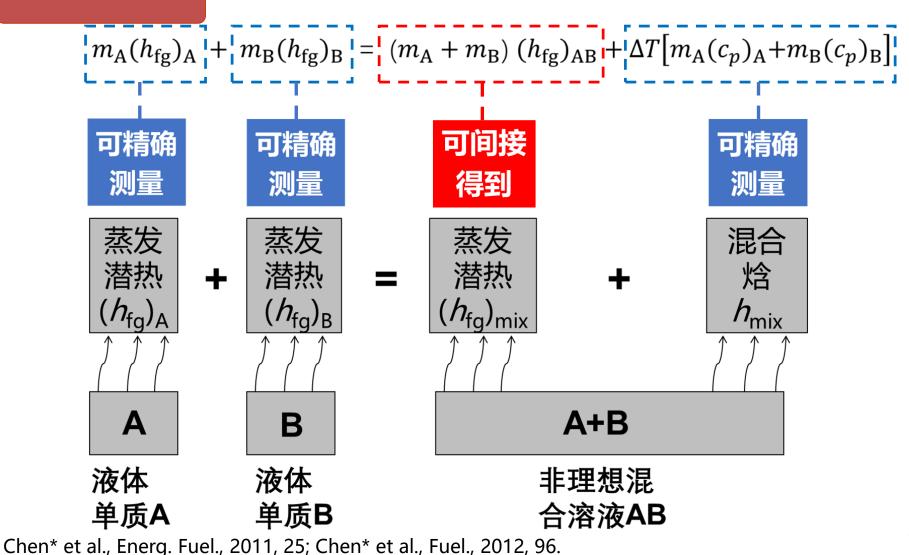
$$f(x_{i}, \theta_{m}, \Psi_{m,n}) = \sum_{k} x_{i} \sum_{k} N_{ki} (Q_{K}RT^{2} \left( \frac{\sum_{m} \theta \Psi_{mk}^{'}}{\sum_{m} \theta \Psi_{mk}^{'}} - \sum_{m} \frac{\theta_{m} \Psi_{k}^{'} m}{\sum_{n} \theta_{n} \Psi_{nm}} - \frac{\theta_{m} \varphi_{km} (\sum_{n} \theta_{n} \Psi_{mn}^{'})}{(\sum_{n} \theta_{n} \Psi_{mn})^{2}} \right) - H_{ki}^{*})$$

Solution

Obtain the latent heat of evaporation indirectly. No need of direct calculation via C-C equation.

**New method** 

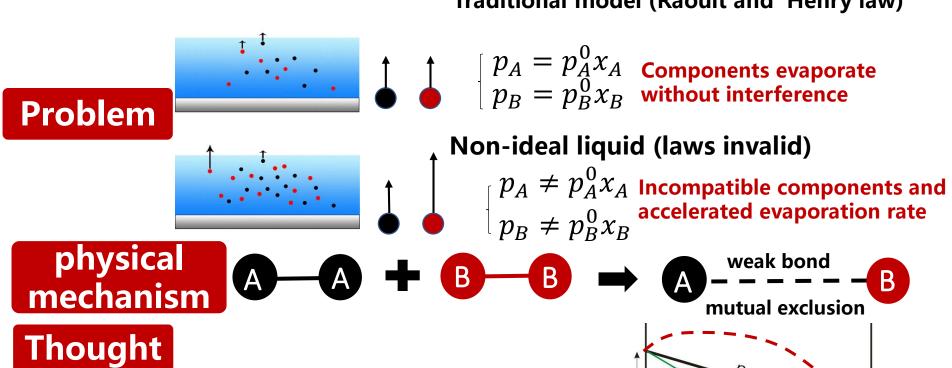
Thermodynamic derivation → Indirect measurement of latent heat



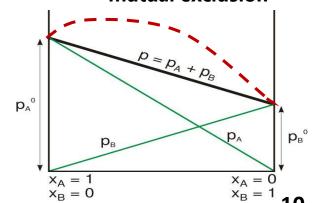
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Reveal the reason for the inaccuracy of vapor component prediction for non-ideal mixtures.

#### Traditional model (Raoult and Henry law)

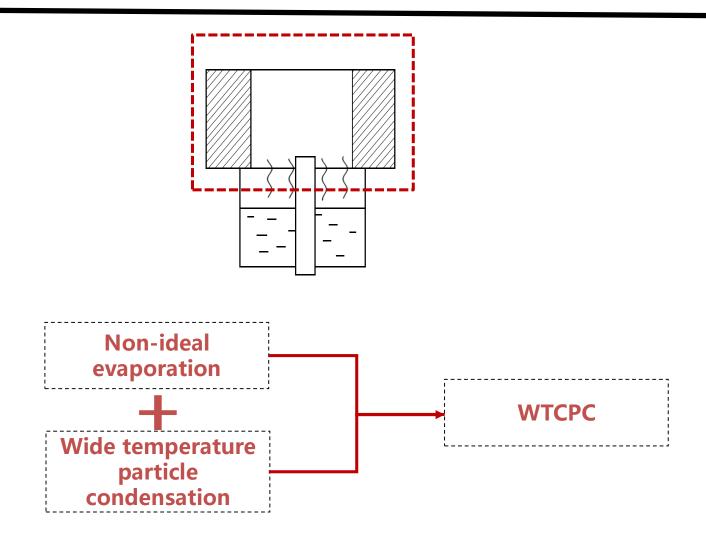


Quantitatively characterize the component evaporation interference, consider the relationship between component page 1 diffusion rate and evaporation rate, establish the unsteady evaporation mechanism (WM,FZ,DC)



Chen\* et al., Int. J. Heat Mass Trans, 2016.

#### **Innovation 2:** Revealing the mechanism of particle condensation growth

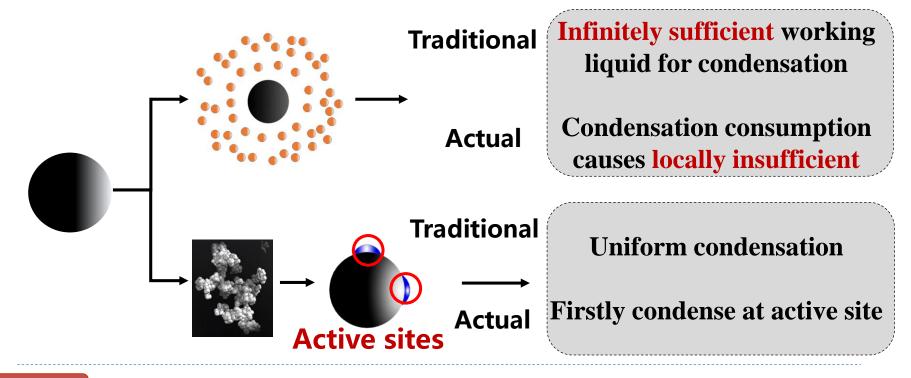


Tackle the uncertainty of predicting particle condensation growth rate.

#### **Innovation 2: Revealing the mechanism of particle condensation growth**

# Question

Prediction of particle condensation rate is inaccurate



# Idea

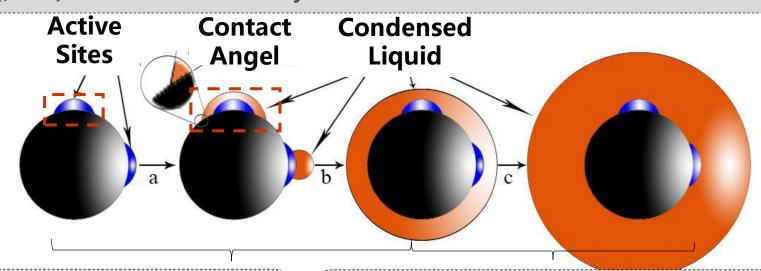
Proposing a multi-stage condensation model incorporating the effects of vapor insufficiency and active sites.

#### **Innovation 2: Revealing the mechanism of particle condensation growth**

#### **New Model**

#### A multi-stage condensation model involving active sites

Active site numbers:  $n = f(\rho, A_p) = \rho n_{p0} z A_{p0} = \rho k_f (\frac{d_g}{d_{p0}})^{D_f} z \pi d_{p0}^2$  $\rho \sim N(\mu, \sigma^2)$ : active site density.



# Heterogeneous

condensation growth rate

$$J = f(\mathbf{n}, J_{hom})$$

$$= K e^{\frac{-\Delta G_{\text{hom}} f(\theta, n)}{kT}}$$

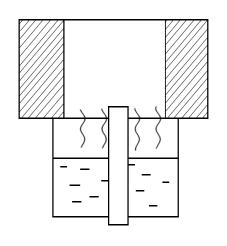
#### **Homogeneous** condensation growth rate

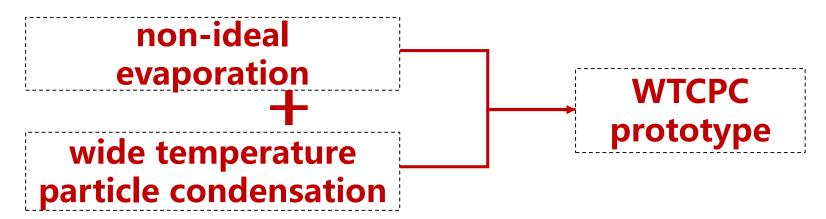
$$J = e^{(A+BT)} K e^{\frac{-\Delta G_{hom}}{kT}} \qquad (d < d_c)$$

$$2\pi D_{no} v_m d_n (P_{co} P_c)$$

$$J = \frac{2\pi D_{vg} v_m d_p}{k} \left( \frac{P_{\infty}}{T_{\infty}} - \frac{P_d}{T_d} \right) f(K n_v) (d > d_c)$$

#### **Innovation 3:** Develop wide temperature condensation particle counter(WTCPC)





**Innovation 3: develop wide temperature CPC (WTCPC)** 

#### **Innovation 3:** Develop wide temperature condensation particle counter(WTCPC)

Challenge

The grown particles are still at high temperature (200°C), and normal photoelectric sensors cannot count them.

1. High temperature causes low SNR of sensors

2. Optical devices would be smeared if we cool down the carrier gas.

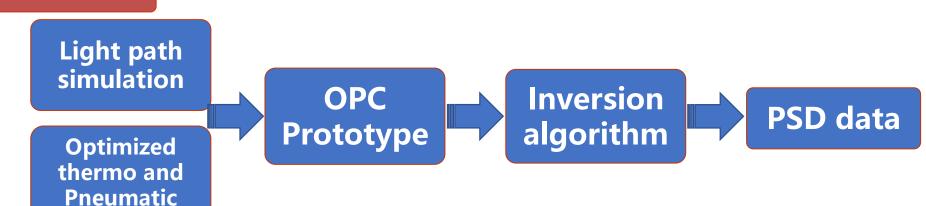
Difficulty



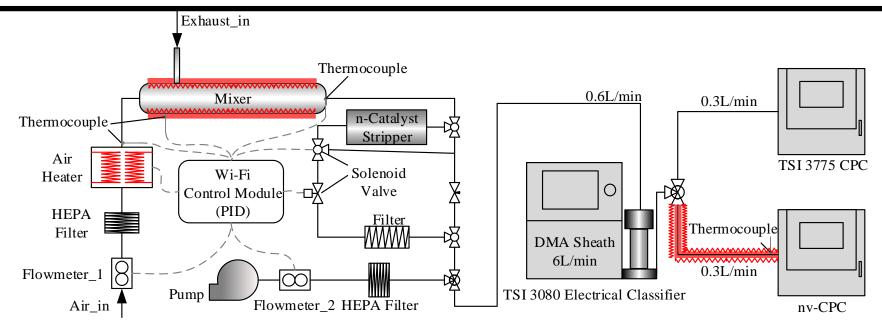




structure



#### Calibration of WTCPC counting efficiency (generating, dilution, counting)





FINAL INTERNATIONAL ISO DRAFT STANDARD 2

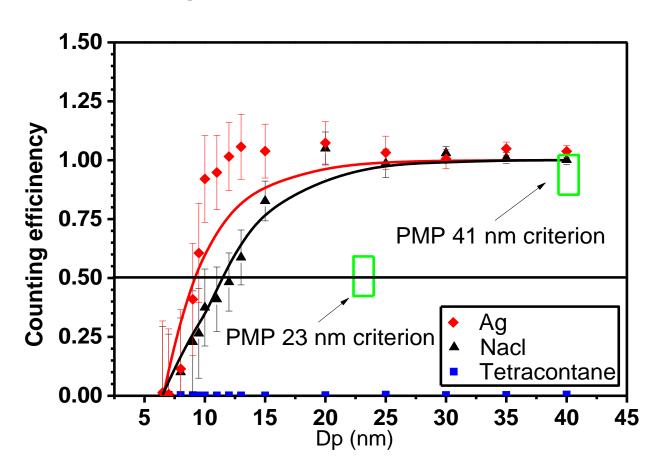
ISO/FDIS 27891

ISO/TC 24/SC 4
Secretariat: DIN
Voting begins on:
2014-07-02
Voting terminates on:

Aerosol particle number concentration — Calibration of condensation particle counters

Densité de particules d'aérosal — Étalonnage de compteurs à

#### Calibration against TSI 3775 CPC as reference



$$d_{90, NaCl} = 20 \text{ nm}$$
  
 $d_{90, Ag} = 16 \text{ nm}$ 

$$d_{50,NaCl}$$
 = 12 nm  $d_{50,Aq}$  = 10 nm

A new version WTCPC is being developed to meet PN10 requirement.

# Summary



	Existing CPC (TSI, Grimm etc.)	WTCPC (BUAA)
Temperature	<b>0-50</b> °C	<b>10-200</b> °C
Particle size	1-1000 nm	10-1000 nm (size bins)
Pre-conditioning	Need cooling	No need of cooling

Aiming at counting PN at high temperature, a new working liquid was designed and associated non-ideality effects were investigated to develop a WTCPC with higher measurement reproducibility.