

# Potential Issues Related to the Measurement of PN During Regeneration of NRMM

A Discussion Document for the PMP WG

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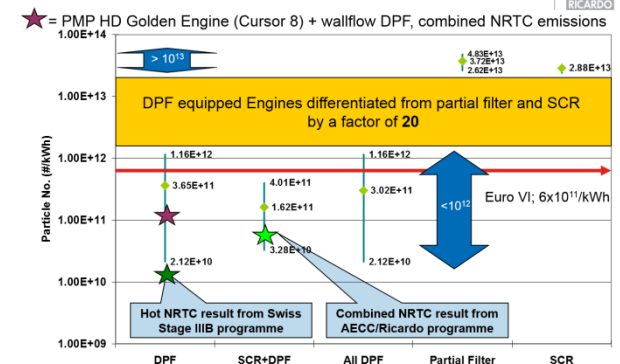
Confidential **EU-JRC (Ispra)**

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Approved



Particle number spread – combined WHTC



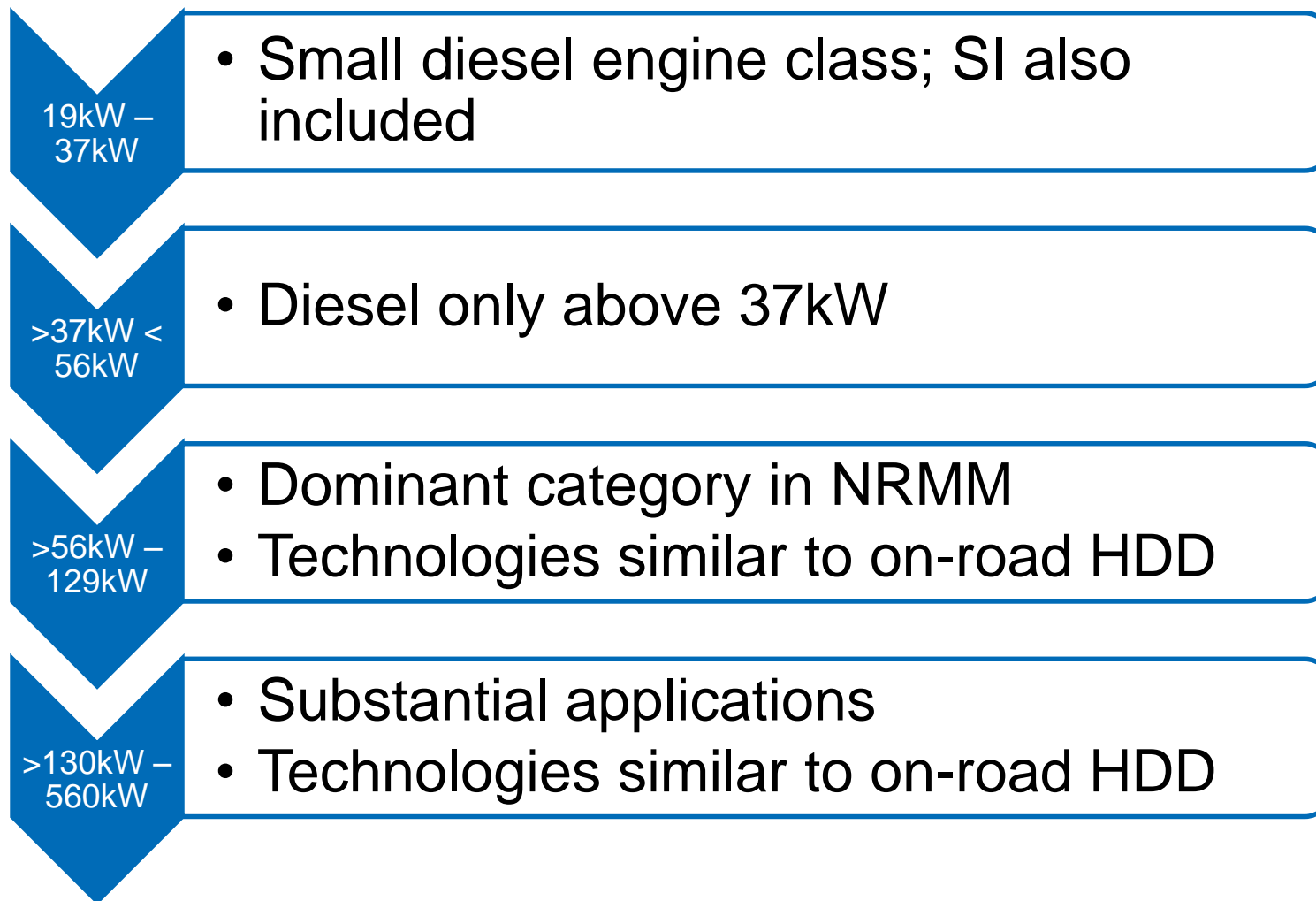
Data from presentation by PMP Chairman to European Commission and Stakeholders

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- Stage V limit value: What factors need to be considered?
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# Introduction

- The document is produced to meet the following objectives regarding gasoline fuelled vehicles:
  - “To identify key influences and issues likely to be encountered in procedures used to measure PN from NRMM
  - Generation of diagrammatic representation of issues and/or annotated table of influences

## NRMM Categories considered for PN legislation

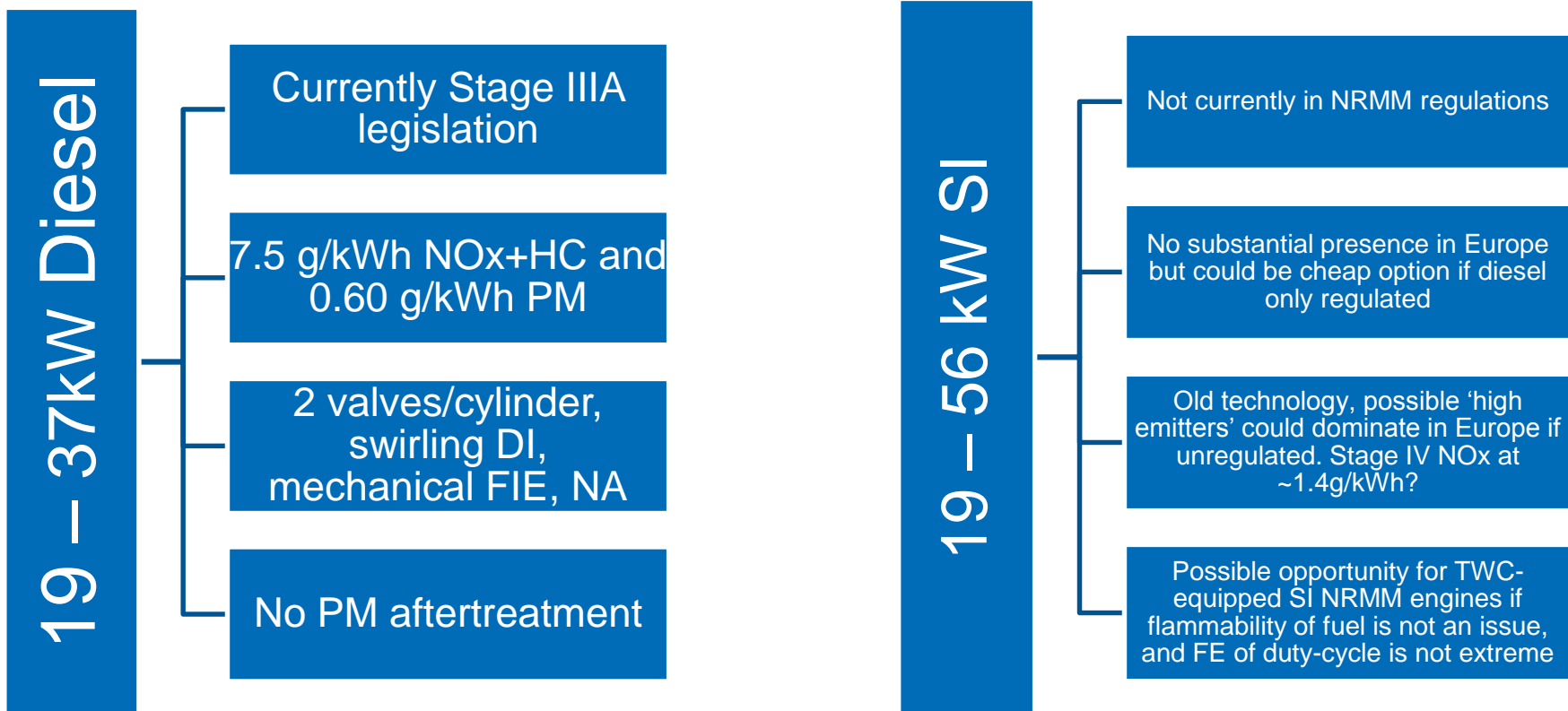


# NRMM Emissions Limits – Stages IIIA to IV

Category	Net Power [kW]	CO [g/kWh]	HC [g/kWh]	NOx [g/kWh]	PM [g/kWh]	Type Approval	New Registration <sup>(1)</sup>
<b>Stage III A (V) = Variable Speed, (C) = Constant Speed</b>							
H (V)	130 ≤ P < 560	3.5	NOx + HC: 4.0		0.2	30 Jun 05	31 Dec 05
H (C)						31 Dec 09	31 Dec 10
I (V)	75 ≤ P < 130	5.0	NOx + HC: 4.0		0.3	31 Dec 05	31 Dec 06
I (C)						31 Dec 09	31 Dec 10
J (V)	37 ≤ P < 75	5.0	NOx + HC: 4.7		0.4	31 Dec 06	31 Dec 07
J (C)						31 Dec 10	31 Dec 11
K (V)	19 ≤ P < 37	5.5	NOx + HC: 7.5		0.6	31 Dec 05	31 Dec 06
K (C)						31 Dec 09	31 Dec 10
<b>Stage III B</b>							
L	130 ≤ P < 560	3.5	0.19	2.0	0.025	31 Dec 09	31 Dec 10
M	75 ≤ P < 130	5.0	0.19	3.3	0.025	31 Dec 10	31 Dec 11
N	56 ≤ P < 75	5.0	0.19	3.3	0.025	31 Dec 10	31 Dec 11
P	37 ≤ P < 56	5.0	NOx + HC: 4.7		0.025	31 Dec 11	31 Dec 12
<b>Stage IV</b>							
Q	130 ≤ P < 560	3.5	0.19	0.4	0.025	31 Dec 12	31 Dec 13
R	56 ≤ P < 130	5.0	0.19	0.4	0.025	30 Sep 13	30 Sep 14

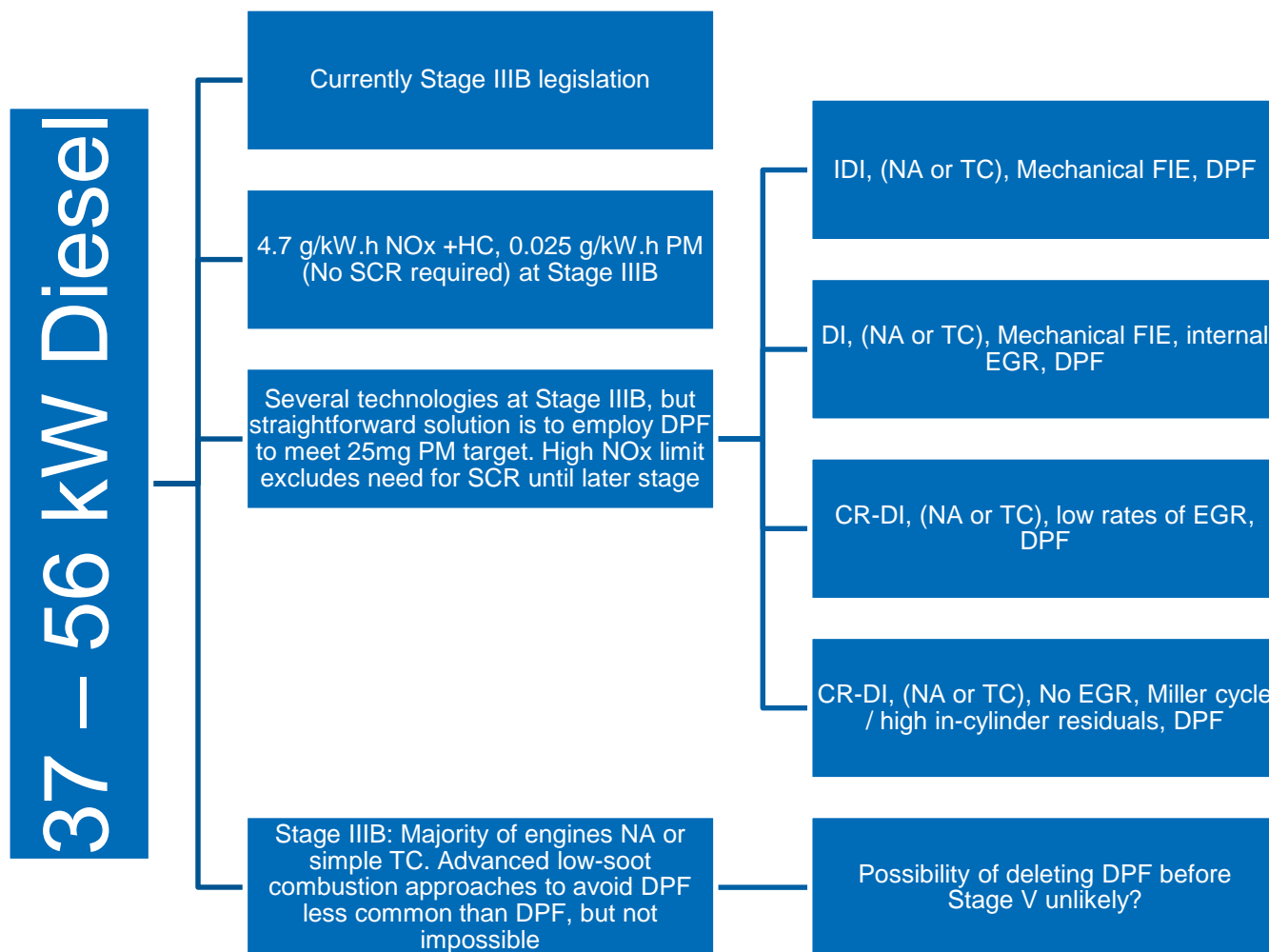
- Introduction of PN limit at 10<sup>12</sup>#/kWh (?) at Stage V

# <37 kW engines currently subject to earlier stage of NRMM regulation or, for SI, none!



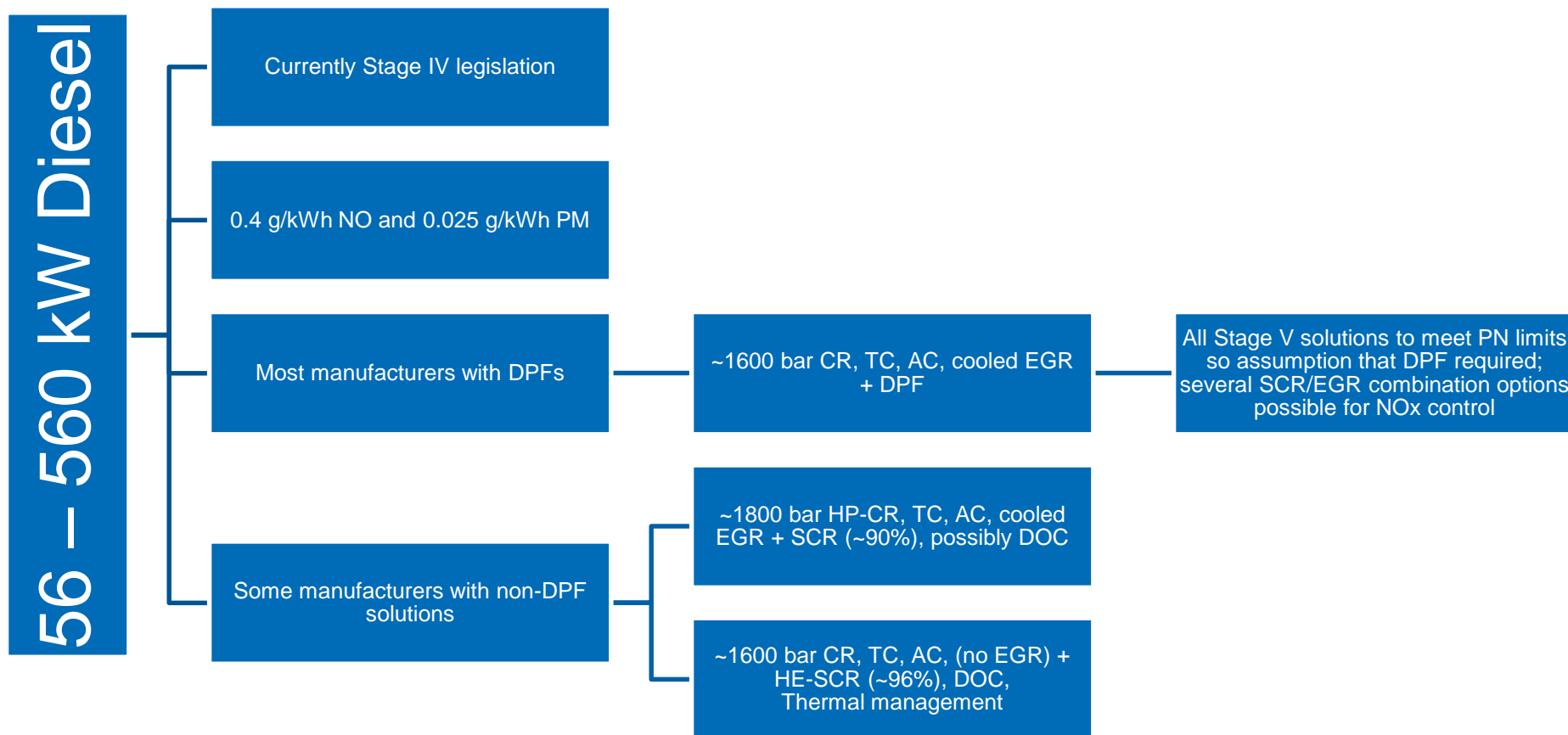
- Major technological changes and cost impact for diesel to meet Stage IV/V NOx and PM
- Potential opportunity for SI applications?
- PN data scarce for this category, especially SI

# 37-56kW engines encompass a wide variety of technologies, currently Stage IIIB regulations



- NOx aftertreatment (SCR) requirement will be the challenge for 37-56kW at next regulatory stage; longer term technology & AT requirements to converge with higher power classes. PN data scarce

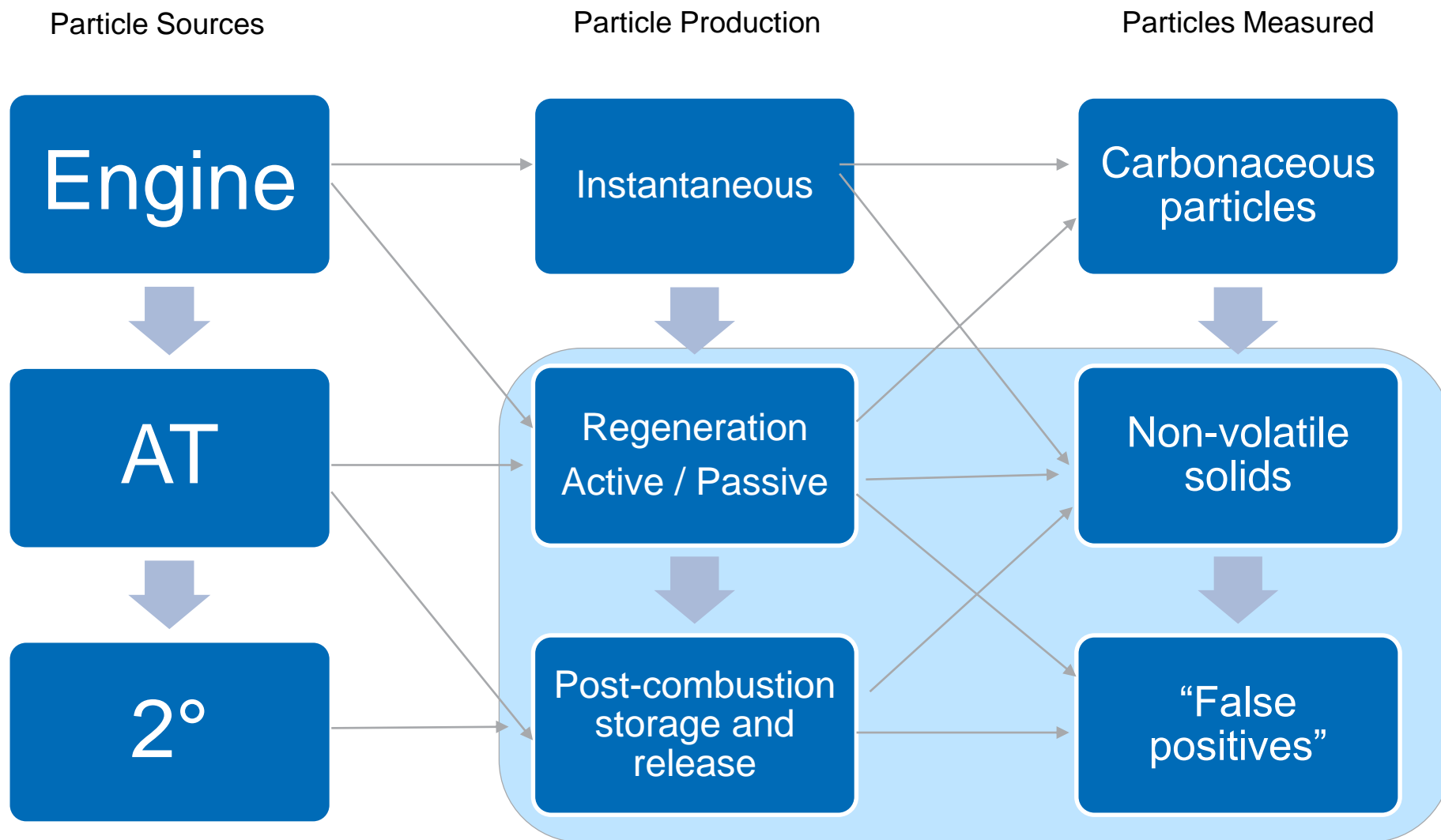
# 56kW to 129kW engines; 130kW to 560kW engines



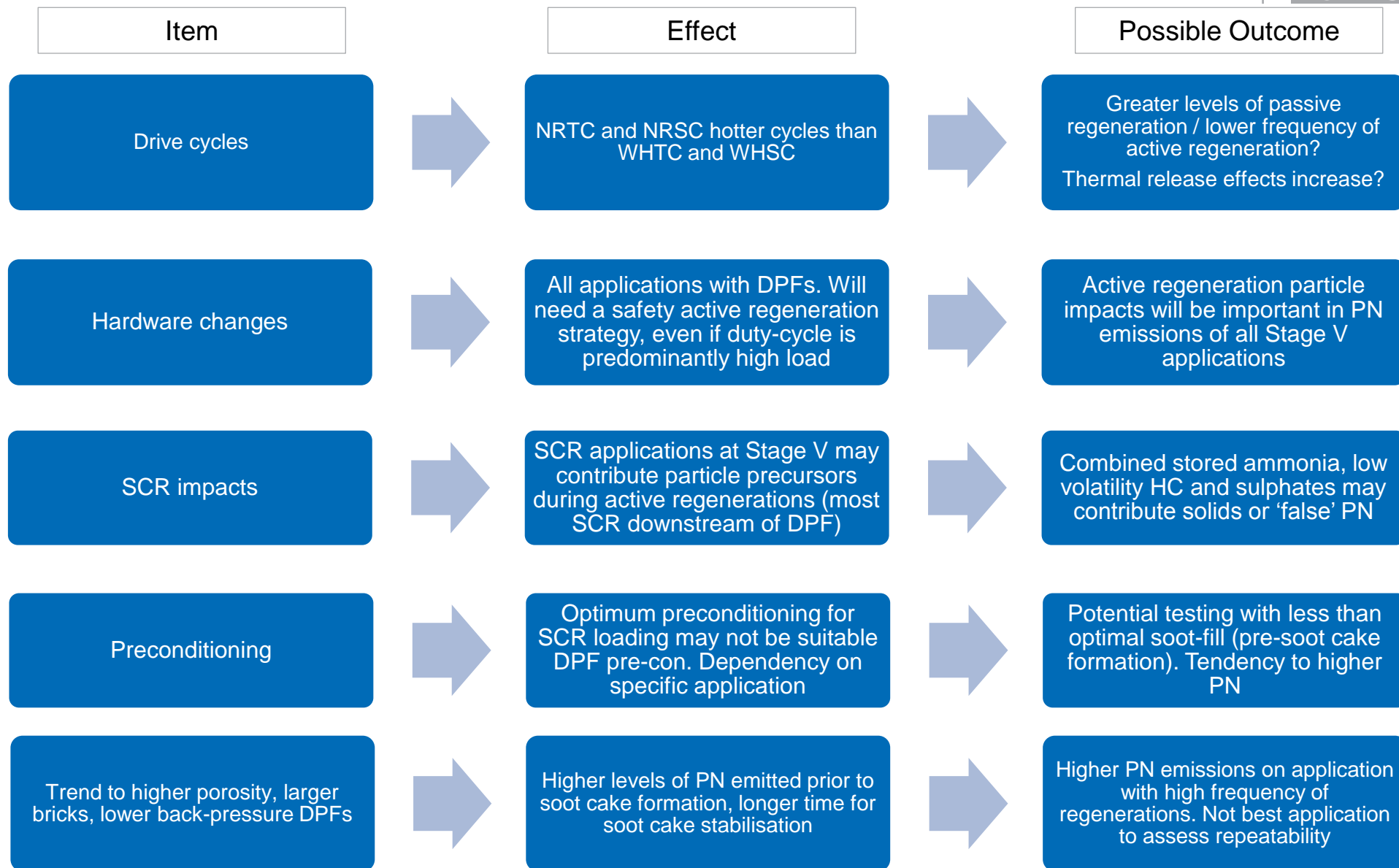
- Stage V >56kW -560kW, engine and AT solutions are converging with on-road HD technologies
- Increase in hybridisation in 130kW to 560kW class; Possible OCV in 130kW to 560kW class?
- Scarce PN data >130kW class



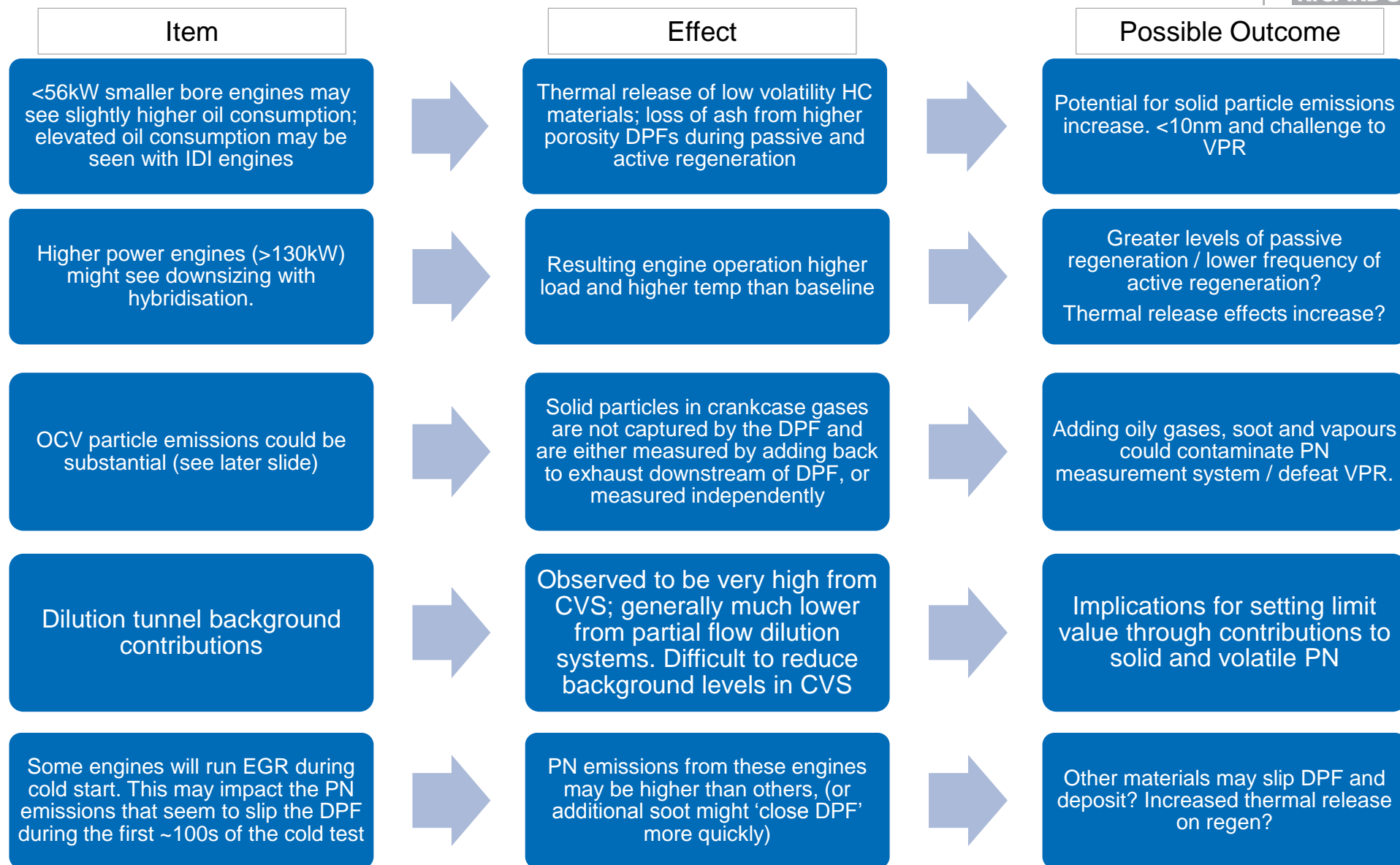
# Particles from engines – sources and influences on regulatory procedures



# General influences on PN / Regenerations from NRMM

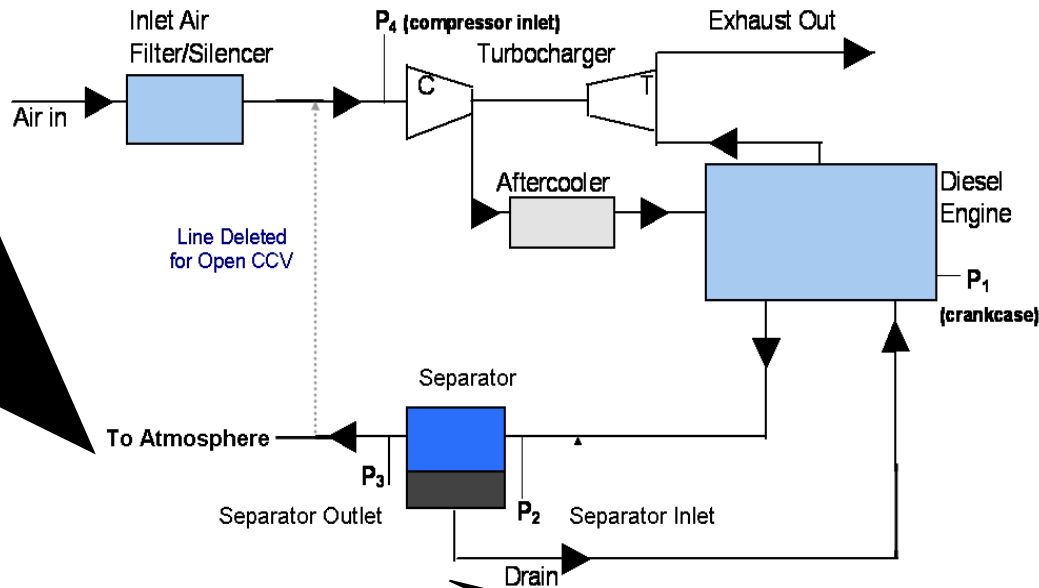


# Specific influences



# Particle Transport In and Emissions from an Open Crankcase Ventilation System

- No influence on engine-out solid PN
- Particles lost to the environment could be as high as 50% of a  $10^{12}\#/kWh$  limit
- This should be possible to investigate experimentally



Blow-by aerosol is vented to atmosphere after filtration. If blow-by flow is 150l/min and exhaust flow is approx (1900rpm x 12 litres) 22800l/min, then PN emitted here will be ~0.7% of EO levels. So, at an EO level of  $10^{14}/kWh$ , PN emitted will be  $7 \times 10^{11}/kWh$ . These levels are similar to post-DPF exhaust levels. The efficiency of the separator for submicron particles might be as low as 50%, so vent emissions of solid particles could be as high as ~50% of a  $10^{12}\#/kWh$  limit

**Assume 12l engine at 1900rpm:**  
 Flow out of the crankcase is ~150l/min (max) and crankcase volume is c. 30 litres. Hence max residence time is ~10s. Temp drops from ~120°C to 80°C. Crankcase aerosol comprises exhaust plus oil plus headspace vapours. It has ~5s to evolve, so time for:  
 •Soot to combine with oil  
 •HC condensation  
 •Oil droplet coagulation  
 •Water condensation

CCV device / PCV valve  
 Entry temp is ~80°C. Pressure drop ~30mb so some revolatilisation may occur. Large oil droplets are mechanically recovered. Most particles of <500nm will remain entrained. Aerosol exits at 60°C

## Particles from NRMM gasoline-fuelled engines

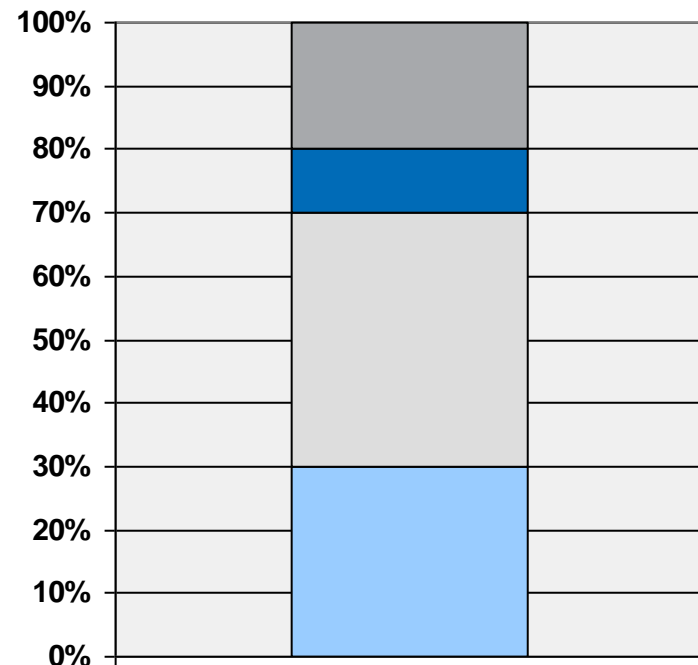
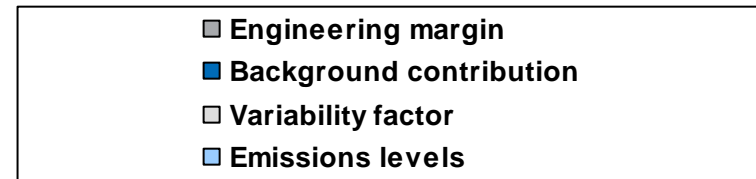
- Presumably stoichiometric with TWC
- PM/PN largely unmeasured and not well understood
- Analogous to on-road position
  - Potential for non-GPF solution?

# Measurement System Influences

- Dilution systems
  - Euro VI gives partial flow and full flow dilution systems equal status, but for NRMM:
    - Impractical to use a full-flow system on a 560kW engine
    - Partial flow systems should be ok for engines down to 19kW
    - (Full flow dilution systems would be needed if <19kW engines were to be tested)
    - Better to mandate partial flow for all applications?
- Crankcase gases
  - OCV presents challenges for PN emissions and measurement
    - Vent emissions levels could be between  $10^{11}$  and  $10^{12}$ #/kWh before considering tailpipe emissions
    - Measurement would either
      - Recombine vent gases (soot/HC/oil mist) with exhaust downstream of the DPF
        - Potential contamination of PN system / challenge to VPR
      - Analyse vent gases independently
        - 2 sets of analysers for gases, PM and PN

# Stage V limit value: What factors need to be considered?

- Emissions levels
  - Representative emissions levels from engine and emissions control technologies
  - Engine-out PN plus DPF filtration efficiency / porosity
- Variability
  - Repeatability of the engine and measurement system
  - Emissions cycle used for certification
  - DPF Regeneration / Ki factor
- Contribution of the background
- Engineering margin
- Existing regulations for other engine types



Possible contributions to PN Limit

## Measurement variability is a critical factor

- Data collected using the regulatory measurement approach
  - Repeatability
    - Over specific emissions cycle
    - Assume no active regeneration of the DPF
    - May include passive regeneration
    - Based upon standard deviation of repeat measurements
  - Active regeneration
    - During specific emissions cycle
    - Determine contribution relative to regeneration periodicity (Ki)
  - Total contributions of variability factors may be greater than the contribution of the measured emissions level
- NRSC and NRTC to be considered
- High temperature operation may lead to passive regeneration, altering the fill state of the DPF and the emissions levels observed
- Active regeneration contributes particles generated in real-time as the soot combusts, and afterwards with the reduced filtration efficiency of the DPF



## Areas for further study

- Active and passive regenerations
  - Real-time PN emissions
  - Effects of thermal release of heavy HC (oil consumption etc) and other volatiles from DOC and DPF
  - Possible impacts of released SCR deposits
- Preconditioning effect on cold start emissions
- Impacts of EGR
- Effects of differences in DPF substrate filtration characteristics on PN emissions
- PN from engines with OCV: absolute levels and how to measure
- Impacts of downsized engines / hybrids
- PN from SI engines