

Study on Low~High temperature test

Prepared by Japan
18th WLTP-IWG
18-20 April 2017

Overview of the study

- Purpose: Evaluate the impact of temperature on Emissions and F.E.
- Test vehicles: ICE vehicle and NOVC-HEV
- Test cycle: WLTC-3 phase (LMH)
- Temperature: 5 conditions, (-7°C, only ICE), +5°C, +14°C, 23°C, 30°C
- A/C setting: A/C OFF, 25-AUTO

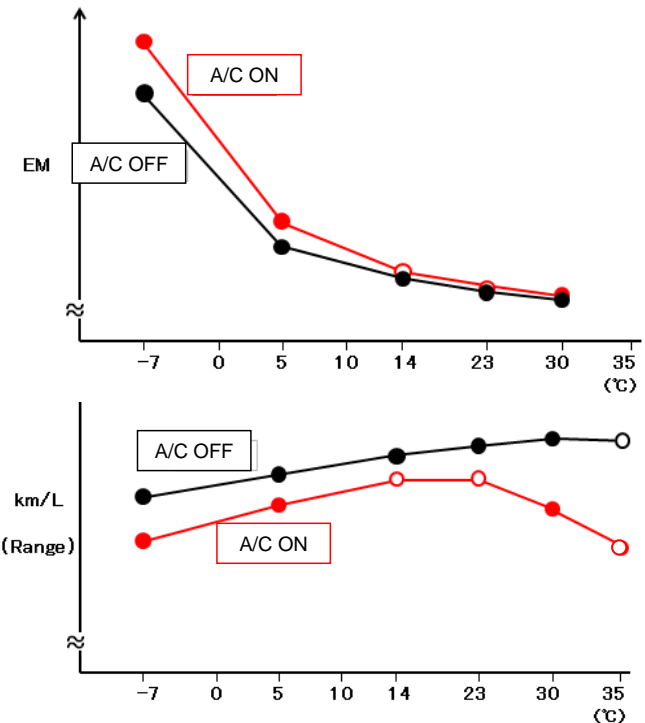
◆ Test matrix

| Vehicle type | A/C operation | Environmental condition | | | | |
|--------------|---------------|-------------------------|-----|------|------|------|
| | | -7°C | 5°C | 14°C | 23°C | 30°C |
| ICE | A/C OFF | 1 | 2 | 2 | 1 | 1 |
| | 25-AUTO | 2 | 2 | - | - | 2 |
| NOVC-HEV | A/C OFF | - | 1 | 1 | 2 | 1 |
| | 25-AUTO | - | 1 | - | - | - |

*) RCB correction factor in each temp. were measured for NOVC-HEV

*) Dynamometer set value was compensated both F0 and F2.

◆ Image of test results



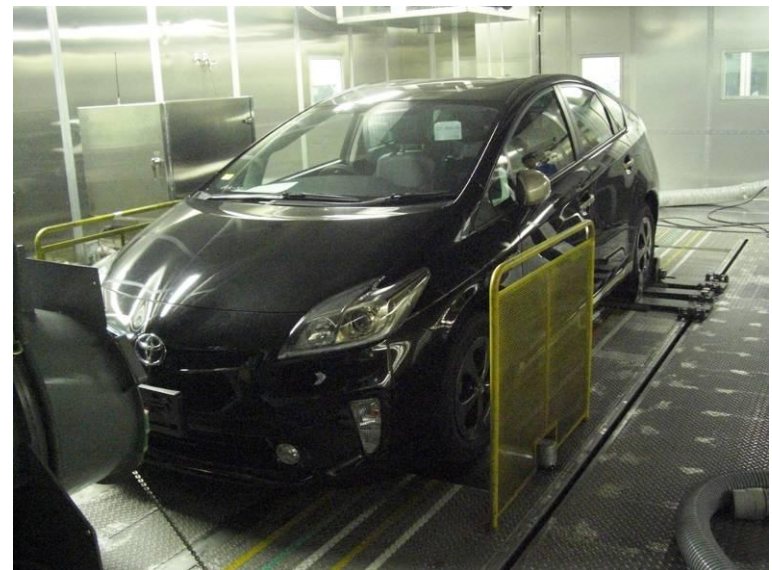
Test vehicles

| Vehicle ID | | ICE | NOVC-HEV |
|--|---|---|--|
| Vehicle category: M1/N1 | | M1 | M1 |
| Vehicle Model | | DBA-GK5 | DAA-ZVW30-AHXEB |
| Body | Length | mm | 3,955 |
| | width | mm | 1,695 |
| | height | mm | 1,525 |
| | Wheelbase | mm | 2,530 |
| | Curb mass under JP regulation - individual | kg | 1,070 |
| | Weight for Tire and tool | kg | 8 |
| | Curb(Unladen) mass under EU regulation (UM) | kg | 1075 |
| | Mass in Running order | kg | 1150 |
| | Riding capacity | persons | 5 |
| | Maximum pay load | kg | 0 |
| | Gross vehicle weight | kg | 1,345 |
| | Technically permissible maximum laden mass (LM) | kg | 1,602 |
| | Mass of the optional equipment of vehicle H | kg | 10 |
| Test mass HIGH | kg | 1,248 | |
| Inertia weight under WLTP - Heaviest-Worst for 2WD-CHDY | kg | 1,265 | |
| Volume of Fuel tank | L | 40 | |
| Engine type | - | L15B | 2ZR-FXE |
| Fuel type (Diesel/Gasoline/LPG) | - | Gasoline-Regular | Gasoline - Regular |
| Engine features | - | Inline-four cylinder engine, Electronic fuel injection, Idle stop, Variable valve timing control device, Electric power steering system | Inline-four cylinder engine, electronic fuel injection, Idle stop, Variable valve timing control device, , electric power steering system, Hybrid system, Electronically controlled Continuously Variable Transmission |
| Technology for FE improvement | - | | |
| Engine displacement | cc | 1,496 | 1,797 |
| Compression ratio | - | 11.5 | 13.0 |
| Maximum rated power | kW | 97 | 73 |
| Engine speed at Max. power | min-1 | 6600 | 5200 |
| Maximum torque | Nm | 155 | 142 |
| Engine speed at Max. torque | min-1 | 4600 | 4000 |
| Engine speed at Idling | min-1 | 700 | 1000 @ Maintenance mode |
| Exhaust-gas after treatment device (TWC, DPF, Urea SCR, etc), Exhaust-gas countermeasure device (EGR, etc) | - | TWC | TWC |
| Motor type | - | - | 3JM |
| Kind of motor | - | - | Permanent magnet AC synchronous motor |
| Rated power | kW | - | 18 |
| Maximum power | kW | - | 60 |
| Motor speed at Max. power | min-1 | - | 2768~4000 |
| Maximum torque | Nm | - | 207 |
| Motor speed at Max. torque | min-1 | - | 0~2768 |
| Type | - | - | NiMH |
| Voltage in each battery | V | - | 7.2 |
| Capacity | Ah | - | 6.5 |
| Number of battery | - | - | 28 |
| Total voltage (Nominal voltage) | V | - | 201.6 |
| Circuit type | - | - | Series |
| Drive system | - | 2D-2 | 2D-2 |
| Transmission type | - | CVT | CVT |
| Transmission | Gear ratio | 1st | - |
| | | 2nd | - |
| | | 3rd | - |
| | | 4th | - |
| | | 5th | - |
| | | 6th | - |
| | | 7th | - |
| | Final drive ratio | - | 4.992 |
| gear ratio (Reverse) | - | 2.706~1.382 | - |
| Tires | Front tire size | m | 185/60R/15 |
| | Rear tire size | m | 185/60R/15 |
| | Dynamic radius of drive tire | m | 0.288 |
| | Pressure | kpa | Fr220 Rr210 |
| Instruments and Controls | Gear shift indicator | Y/N | N |
| | Idling stop system | Y/N | Y |
| Odometer | Cruise control | Y/N | N |
| | | km | 12,000 |
| | | | 101,500 |

◆ ICE vehicle



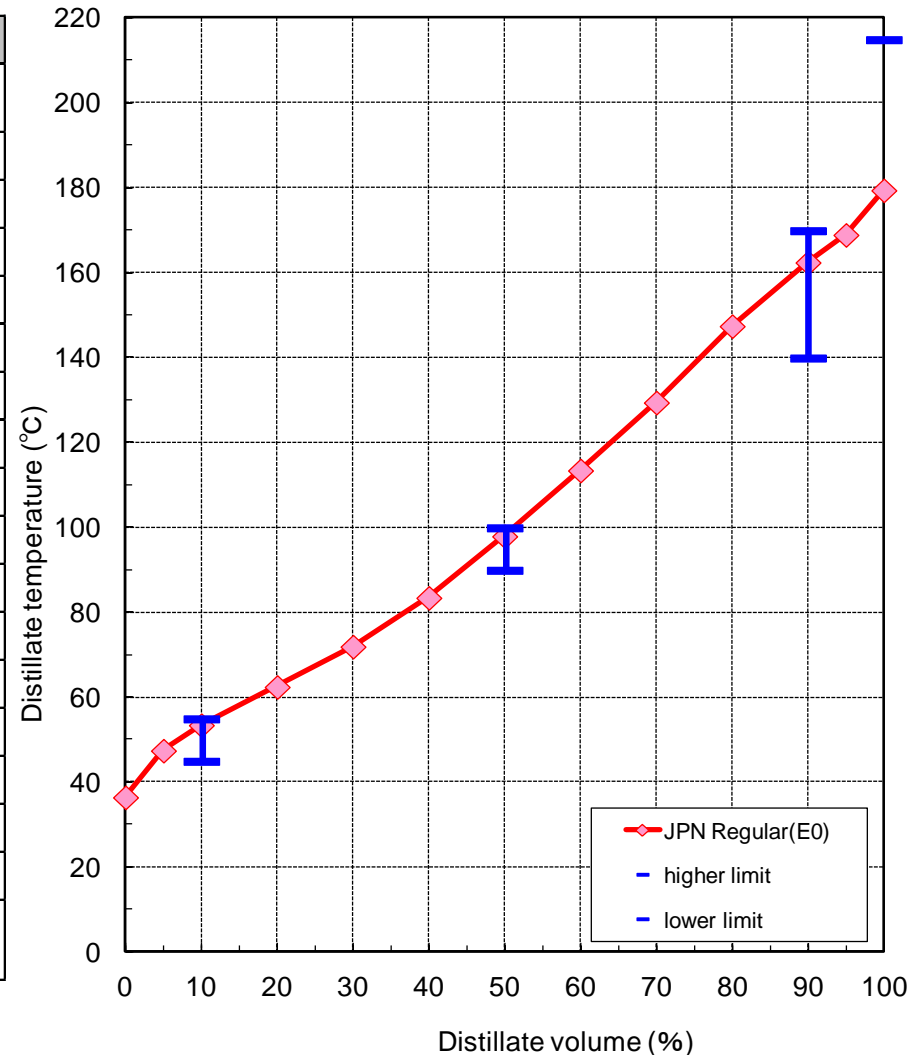
◆ NOVC-HEV



Fuel property

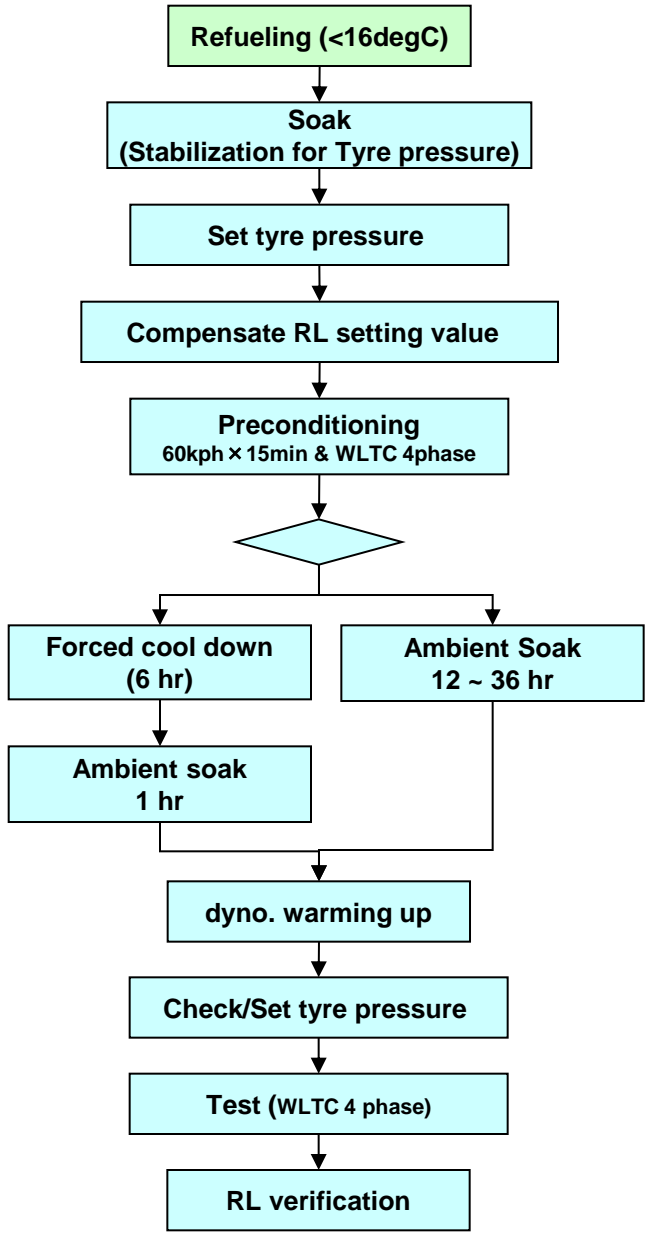
Reference fuel for Japan type approval test was used
(not winter grade fuel)

| Property | | Unit | Value | Method |
|---|---------------------|----------|----------------------|-----------|
| Type of fuel | | - | Gasoline Regulaer | - |
| Density at 15 °C | | g/cm3 | 0.7320 | JIS K2249 |
| Octane number | RON | - | 90.5 | JIS K2280 |
| Distillation: | 10% point | °C | 53.5 | JIS K2254 |
| | 50% point | °C | 98.0 | JIS K2254 |
| | 90% point | °C | 162.5 | JIS K2254 |
| | Final boiling point | °C | 179.5 | JIS K2254 |
| | Residue | vol% | 1.0 | JIS K2254 |
| Vapour pressure (RVP) 37.8°C | | kPa | 58.1 | JIS K2258 |
| Lead content | | g/l | 0.001(-) | JIS K2255 |
| Sulphur content | | mass% | 0.0007 | JIS K2541 |
| benzene | | vol% | 0.4 | JIS K2536 |
| Oxygen content | | vol% | 0.1(-) | JIS K2536 |
| MTBE | | vol% | 0.1(-) | JIS K2536 |
| Methanol | | vol% | 0.1(-) | JIS K2536 |
| Ethanol | | vol% | 0.1(-) | JIS K2536 |
| Kerosene | | vol% | 0.7(-) | JIS K2536 |
| Solvent washed gum (Exsistant gum content) | | mg/100ml | 0 | JIS K2261 |



Test procedure

Room temperature (-7 / 5 / 14 / 30°C)



• JPN fuel for TA

• Compensate dyno. RL set value
(Both F0 and F2)

- Average of 1hr: ±3°C
- Maximum: ±6°C
- 3 minutes: ±3°C

- At start: ±2°C
- Average: ±3°C
- Maximum: ±6°C
- 3 minutes.: ±3°C
- A/C operation: 25-AUTO@-7°C, 5°C, 30°C
- Defroster: OFF
- Cooling fan: speed proportional
- Bonnet: Close

RL Compensation

- ◆ Target RL in each temperature was calculated by the equation in the GTR15 annex4.

$$F_{0_t} = \frac{F_{0_20}}{(1 + 8.6 \times 10^{-3} \times (t - 20))}$$

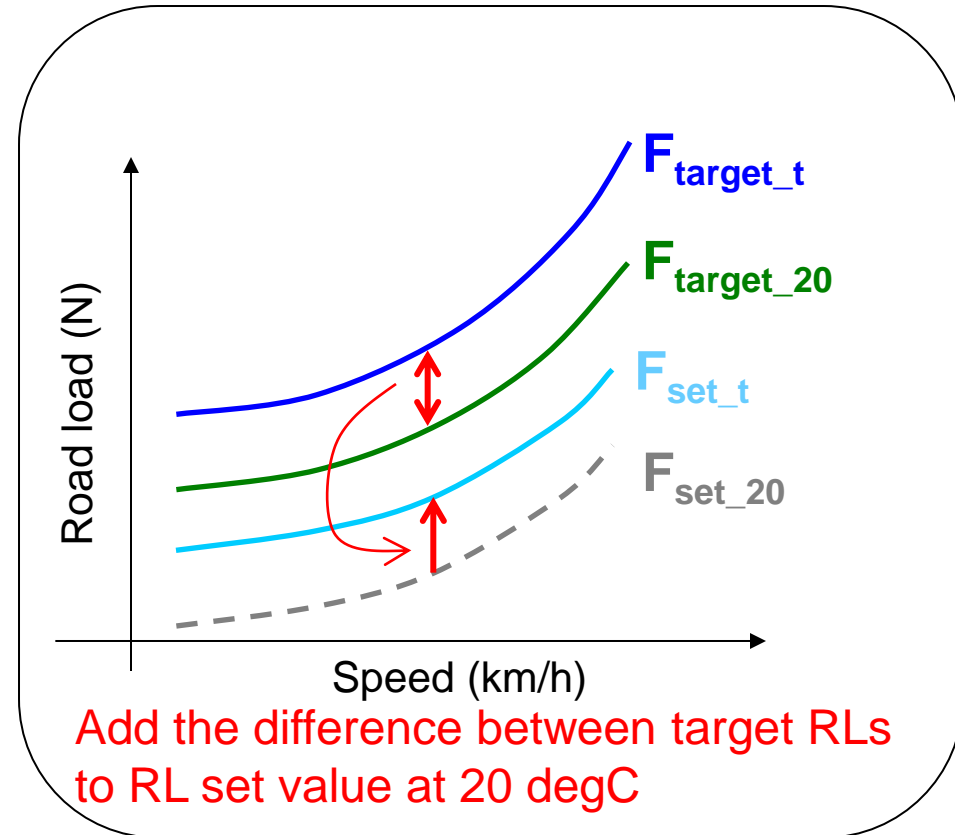
$$F_{2_t} = \frac{F_{2_20}}{((273 + t) / 293)}$$

- ◆ Dyno. set value was compensated.
(Coast down wasn't performed)

$$F_{set_t} = F_{set_20} + (F_{target_t} - F_{target_20})$$

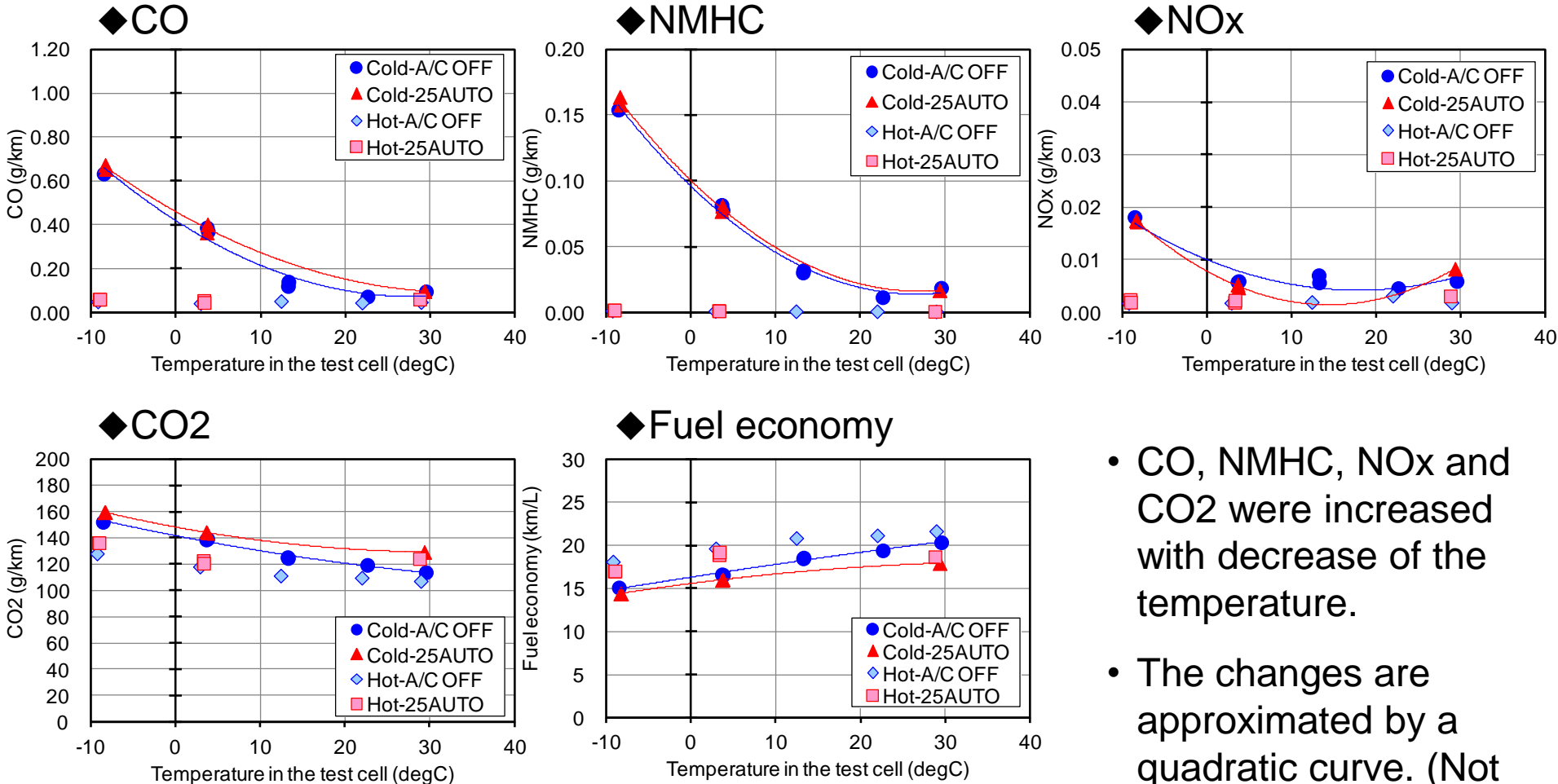
$$F_{target_t} = F_{0_t} + F_{1_t} \cdot v + F_{2_t} \cdot v^2$$

t: test temperature (degC)



Test results of ICE vehicle

<WLTC-LMH>

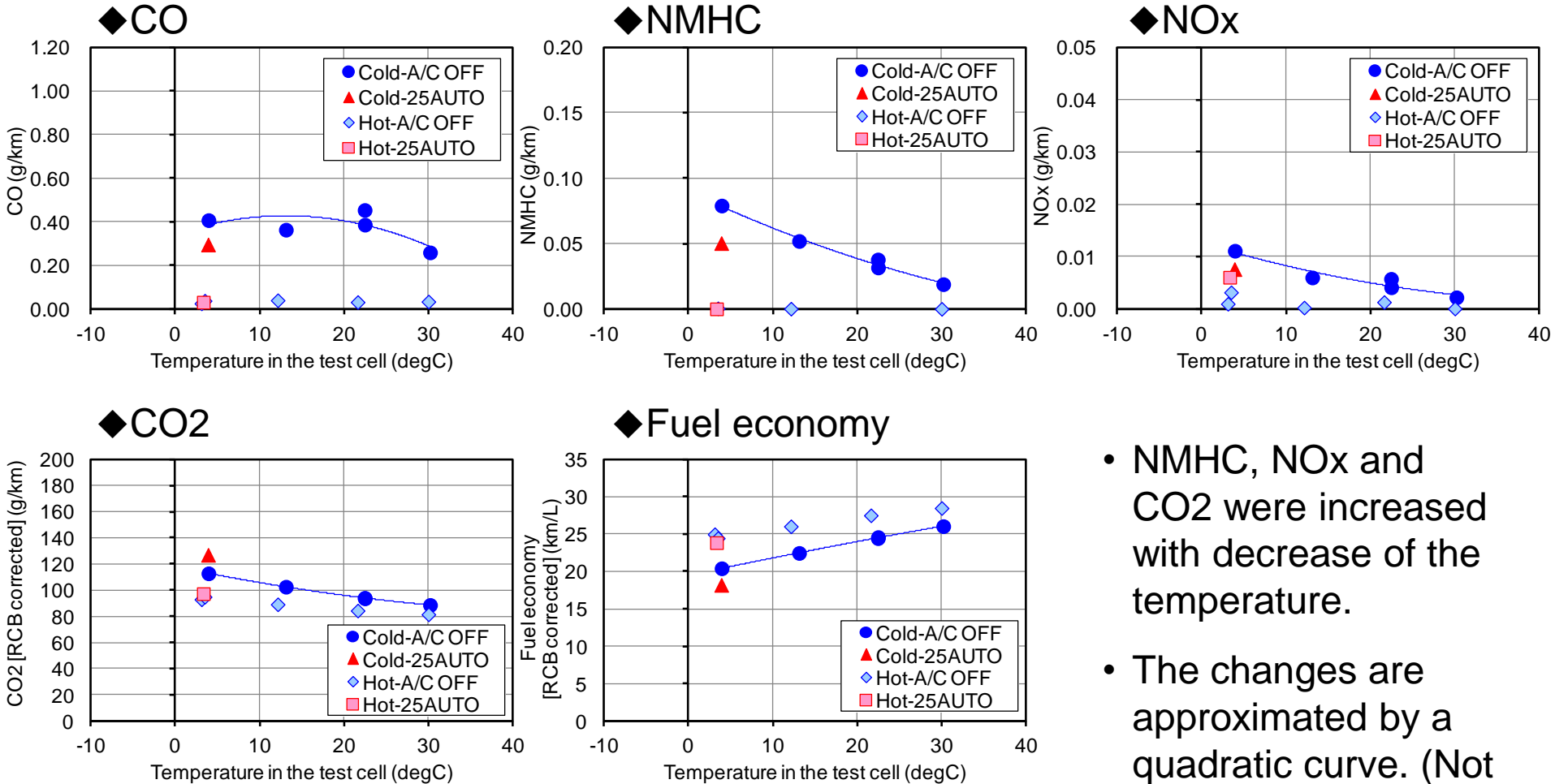


- CO, NMHC, NOx and CO2 were increased with decrease of the temperature.
- The changes are approximated by a quadratic curve. (Not linear)

[NOTE] Emission and F.E were measured during preconditioning and then the results are consider as the hot condition

Test results of NOVC-HEV

<WLTC-LMH>

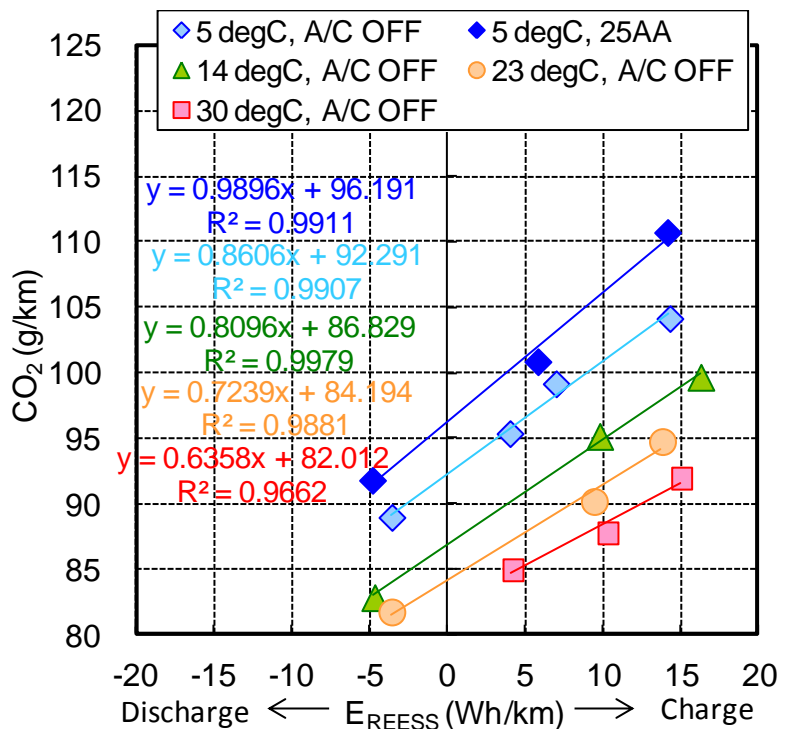


- NMHC, NOx and CO2 were increased with decrease of the temperature.
- The changes are approximated by a quadratic curve. (Not linear)

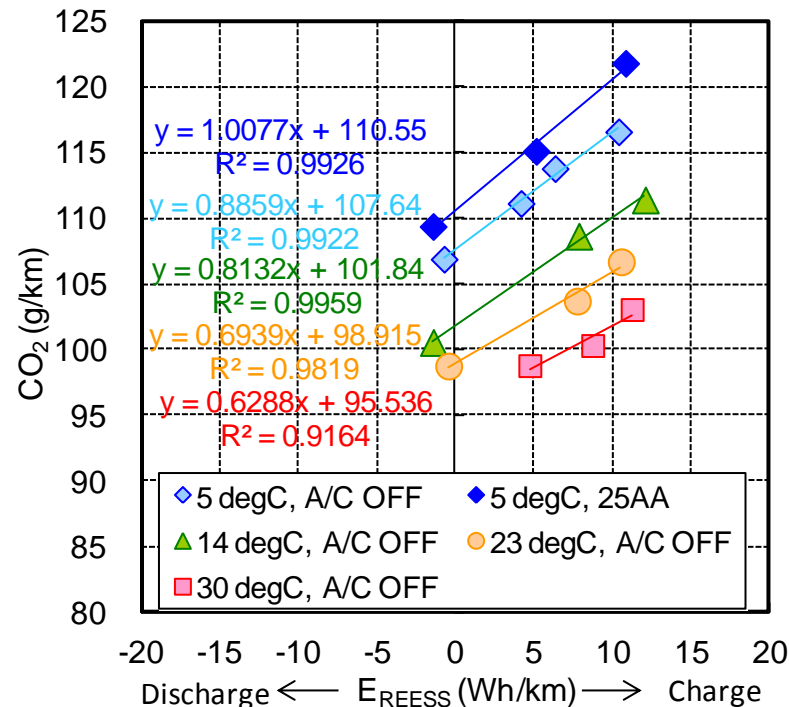
[NOTE] Emission and F.E were measured during preconditioning and then the results are consider as the hot condition

CO2 correction coefficient (measured under Hot condition)

◆ 3 phase



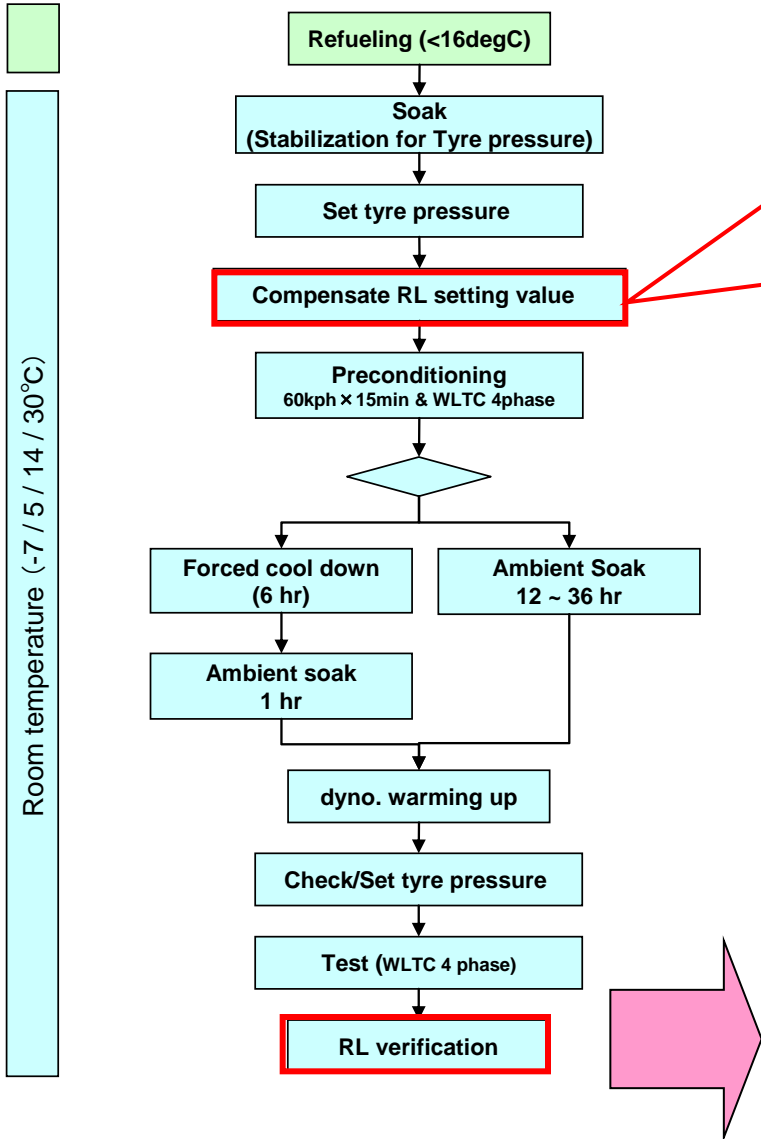
◆ 4 phase



CO2 correction coefficients in each temperature with&without MAC are slightly different.

→ need to consider the balance between test accuracy and testing burden

Confirmation on the set RL



Both F0 and F2 were compensated

RL Compensation WLTP-18-11e

- ◆ Target RL in each temperature was calculated by the equation in the GTR15 annex4.

$$F_{0,t} = \frac{F_{0,20}}{(1 + 8.6 \times 10^{-3} \times (t - 20))}$$

$$F_{2,t} = \frac{F_{2,20}}{((273 + t) / 293)}$$

- ◆ Dyno. set value was compensated. (Coast down wasn't performed)

$$F_{set,t} = F_{set,20} + (F_{target,t} - F_{target,20})$$

$$F_{target,t} = F_{0,t} + F_{1,t} \cdot v + F_{2,t} \cdot v^2$$

t: test temperature (degC)

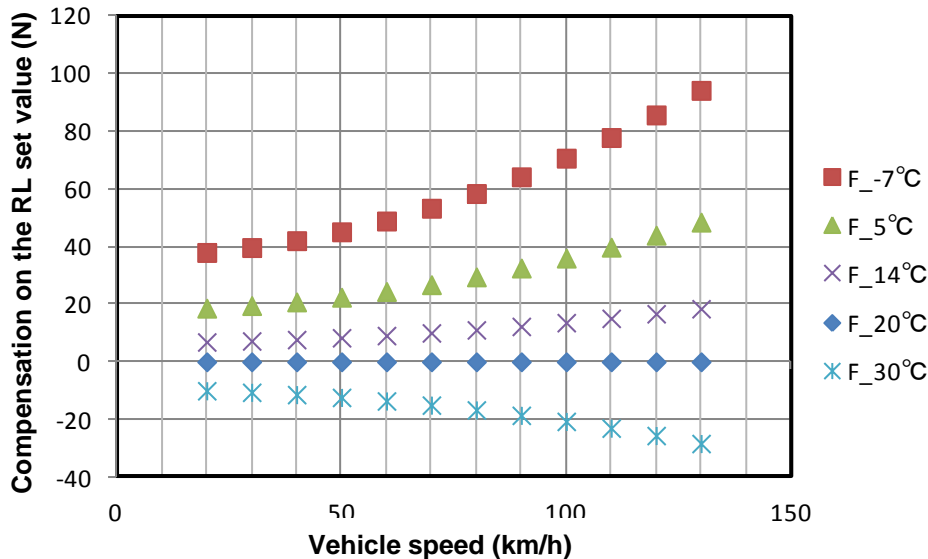
Add the difference between target RLs to RL set value at 20 degC

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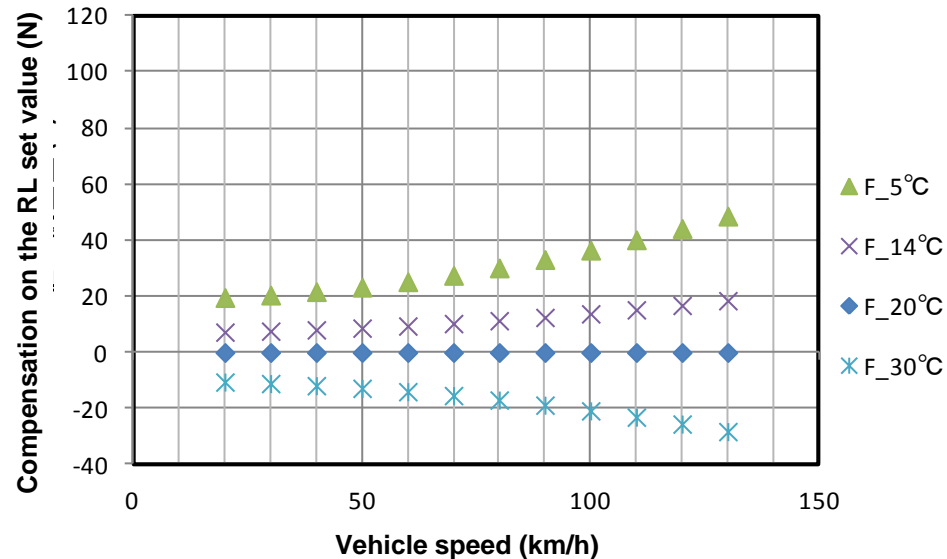
Check the verified RL just after the WLTC test. Then it was compared to the target RL.

Compensation for RL setting value

◆ ICE



◆ HEV



○Detail of compensation
(Rolling resistance and air resistance component)

| | -7°C | | 5°C | | 14°C | | 30°C | |
|-----|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|
| | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ |
| 20 | 37 | 1 | 18 | 1 | 7 | 0 | -10 | 0 |
| 30 | 37 | 3 | 18 | 2 | 7 | 1 | -10 | -1 |
| 40 | 37 | 5 | 18 | 3 | 7 | 1 | -10 | -2 |
| 50 | 37 | 9 | 18 | 5 | 7 | 2 | -10 | -3 |
| 60 | 37 | 12 | 18 | 7 | 7 | 3 | -10 | -4 |
| 70 | 37 | 17 | 18 | 9 | 7 | 3 | -10 | -5 |
| 80 | 37 | 22 | 18 | 12 | 7 | 4 | -10 | -7 |
| 90 | 37 | 28 | 18 | 15 | 7 | 6 | -10 | -9 |
| 100 | 37 | 34 | 18 | 18 | 7 | 7 | -10 | -11 |
| 110 | 37 | 41 | 18 | 22 | 7 | 8 | -10 | -13 |
| 120 | 37 | 49 | 18 | 26 | 7 | 10 | -10 | -16 |
| 130 | 37 | 58 | 18 | 31 | 7 | 12 | -10 | -19 |

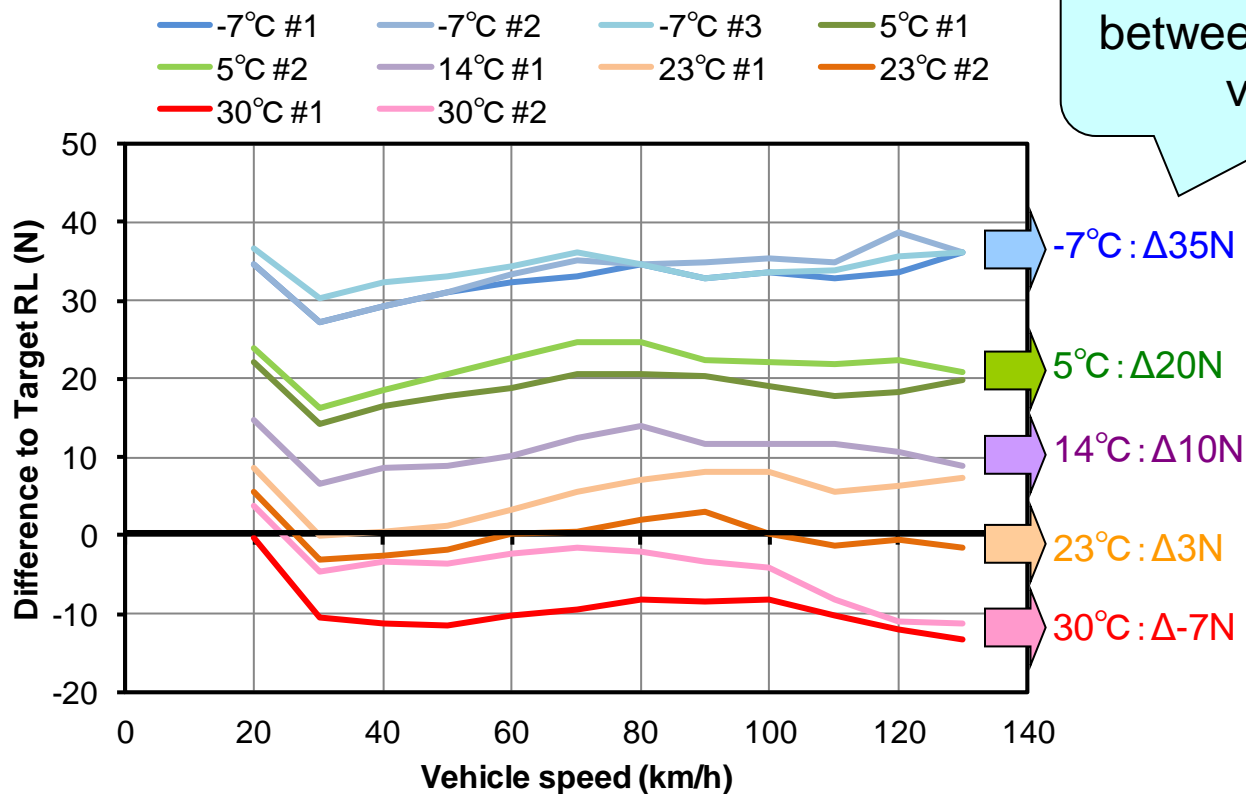
37N
 18N
 7N
 -10N

○Detail of compensation
(Rolling resistance and air resistance component)

| | -7°C | | 5°C | | 14°C | | 30°C | |
|-----|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|----------------|--------------------------|
| | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ | $\Delta \mu_r$ | $\Delta \mu_a \cdot V^2$ |
| 20 | 39 | 1 | 19 | 1 | 7 | 0 | -10 | 0 |
| 30 | 39 | 3 | 19 | 2 | 7 | 1 | -10 | -1 |
| 40 | 39 | 5 | 19 | 3 | 7 | 1 | -10 | -2 |
| 50 | 39 | 8 | 19 | 4 | 7 | 2 | -10 | -3 |
| 60 | 39 | 12 | 19 | 6 | 7 | 2 | -10 | -4 |
| 70 | 39 | 16 | 19 | 9 | 7 | 3 | -10 | -5 |
| 80 | 39 | 21 | 19 | 11 | 7 | 4 | -10 | -7 |
| 90 | 39 | 27 | 19 | 14 | 7 | 6 | -10 | -9 |
| 100 | 39 | 33 | 19 | 18 | 7 | 7 | -10 | -11 |
| 110 | 39 | 40 | 19 | 21 | 7 | 8 | -10 | -13 |
| 120 | 39 | 48 | 19 | 25 | 7 | 10 | -10 | -15 |
| 130 | 39 | 56 | 19 | 30 | 7 | 11 | -10 | -18 |

39N
 19N
 7N
 -10N

The result of RL verification (ICE vehicle)



Average difference
between target RL and
verified RL

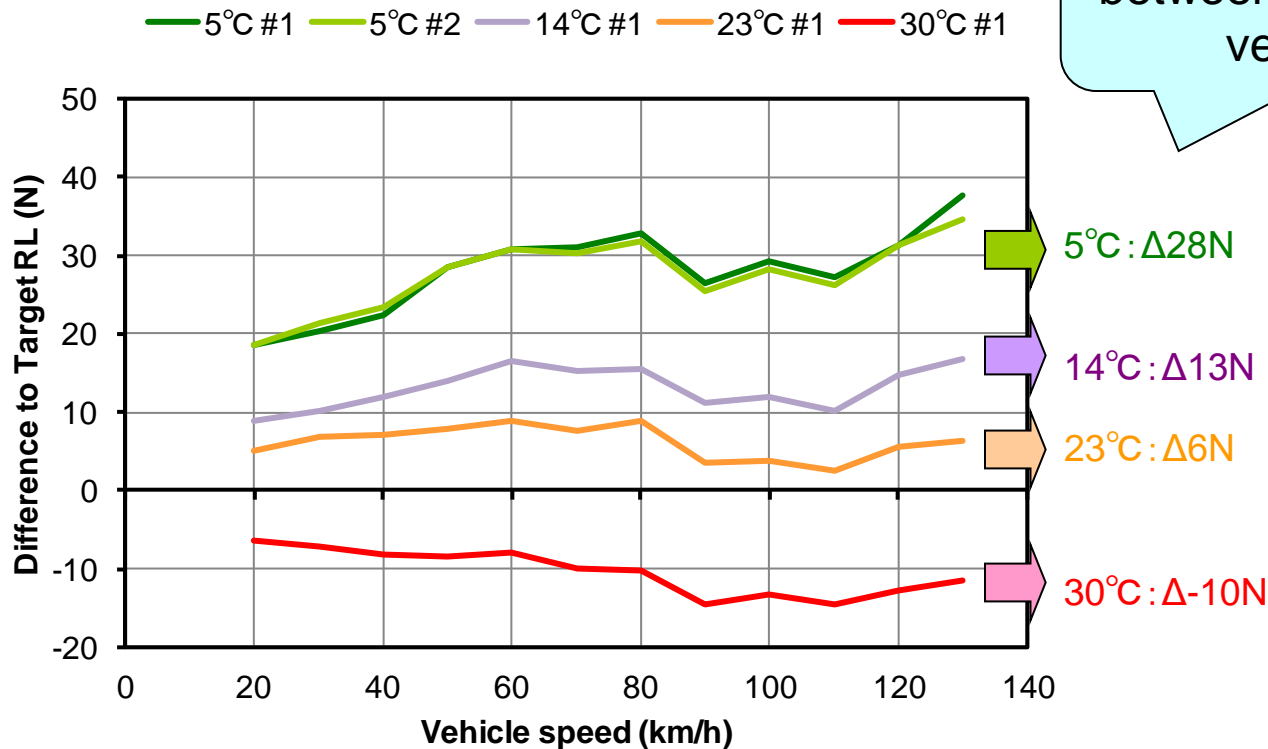
○ Compensation on
rolling resistance

- -7°C: 37N
- 5°C: 18N
- 14°C: 7N
- 30°C: -10N

⇒ The difference between
the target RL and verified
RL is almost same as the
compensated RL of
rolling resistance.

- According to the RL verification (quick check) after the WLTC test, the verified RL was higher than the target RL in low temperature test.
- The difference between the target RL and verified RL are almost identical to the compensated value of rolling resistance component.
- There is a possibility that it is not need to compensate rolling resistance component. (need to further analysis of non-driven wheels component)

The result of RL verification (NOVC-HEV)



Average difference
between target RL and
verified RL

○ Compensation on
rolling resistance

- 5°C : 19N

- 14°C : 7N

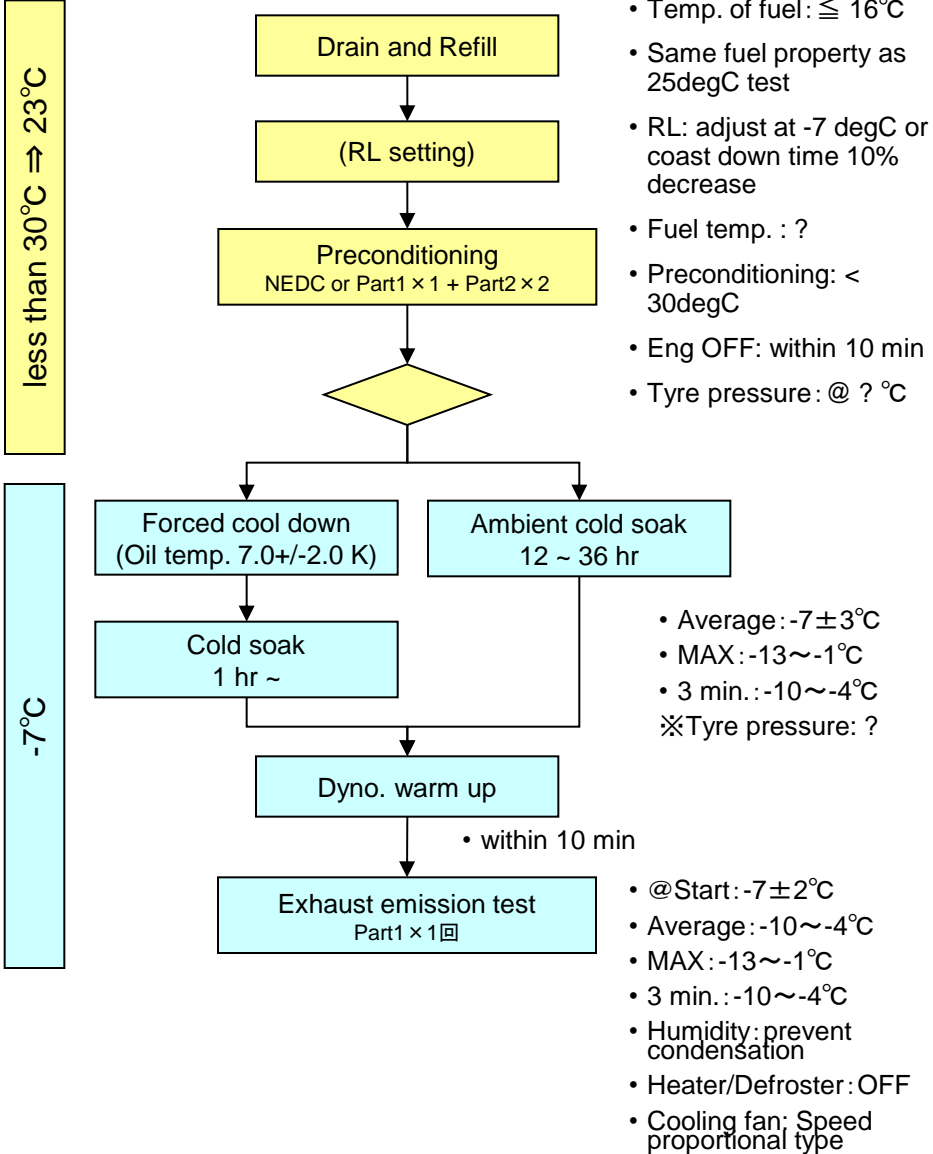
- 30°C : -10N

⇒ The difference between
the target RL and verified
RL is almost same as the
compensated RL of
rolling resistance.

- According to the RL verification (quick check) after the WLTC test, the verified RL is higher than the target RL in this test condition.
- The difference between the target RL and verified RL are nearly identical to the compensated value of rolling resistance component.
- There is a possibility that it is not need to compensate rolling resistance component. (need to further analysis of non-driven wheels component)

(Ref.) Comparison of -7 degC test

UN R83 Annex8



US 40CFR 1066 subpart H

