

10 July 2018

PRESENTATION OF



INTERNATIONAL ORGANIZATION OF MOTOR VEHICLE MANUFACTURERS

**Various Technical Topics  
on the development of ASEP**



# **L<sub>urban</sub>-Assessment**

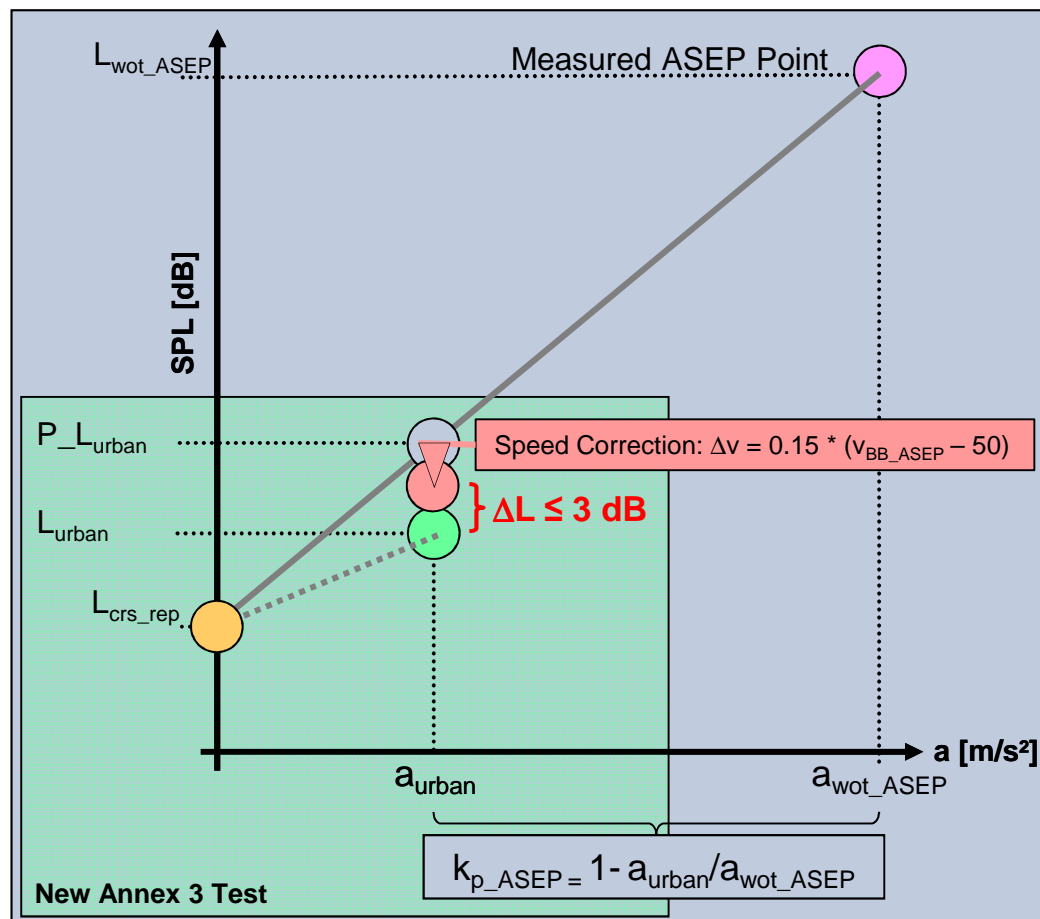
**Informal Working Group ASEP  
Report Paper on**

**Interpretation of ASEP Paragraph 6.2.3 last sentence**

## ***Introduction***

- IWG ASEP has prepared a report paper to provide guidance for the understanding and interpretation of ASEP paragraph 6.2.3 last sentence.
- An explanation is provided for „significant deviation“ in terms of sound, leading to a suggested  $\Delta L_{ASEP}$  of 6 decibel.
- While the  $\Delta L_{ASEP}$  of 6 decibel is directly applied for the „Slope-Assessment“, reduced values are suggested for the alternative assessment method the  $L_{urban}$ -Assessment“.
- This small presentation is intended to provide help for better understanding.

## Concept of the Alternative $L_{urban}$ -Test

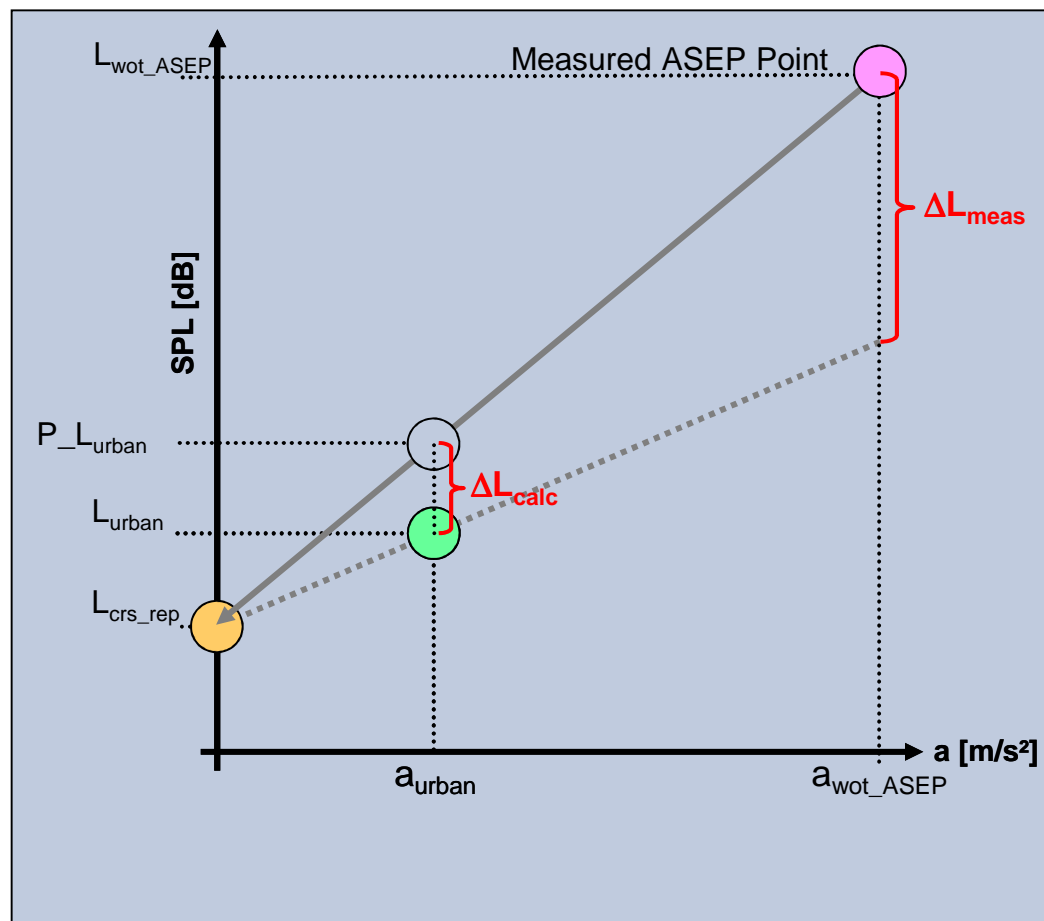


### Flow Chart for Assessment of ASEP using Pseudo $L_{urban}$

- 1 Perform the Type Approval Test according to Annex 3 of ECE R51; Report the following parameter:  
 $a_{urban}$ ;  $L_{urban}$ ;  $L_{crs\_rep}$
- 2 Perform a sound measurement on the test track (operation conditions within the ASEP boundaries)  
Reported results are:  $v_{bb\_ASEP}$ ;  $a_{wot\_ASEP}$ ;  $L_{wot\_ASEP}$
- 3 Calculate the particular partial power factor  $k_p$ :  
 $k_{p\_ASEP} = 1 - a_{urban} / a_{wot\_ASEP}$
- 4 Calculate the Pseudo  $L_{urban}$ :  
 $P_{L\_urban} = L_{wot\_ASEP} - k_{p\_ASEP} * (L_{wot\_ASEP} - L_{crs\_rep})$
- 5 Compensate for the speed influence,  
 $P_{L\_urban\_ASEP} = P_{L\_urban} - 0,15 * (v_{BB\_ASEP} - 50)$
- 6 Check vehicle compliance with ASEP  
 $\Delta L_{ASEP} = P_{L\_urban} - L_{urban} \leq 3 \text{ dB}$

The method allows to assess individual runs. Step 2 to step 6 have to be repeated after every test run.

## Concept of the Alternative $L_{urban}$ -Test



A measured sound level  $L_{wot\_ASEP}$  is rated in the  $L_{urban}$  method according to the acceleration performance that has been achieved in that particular test condition.

The higher the acceleration, the lower the evaluation values for that single point.

$$\frac{L_{wot\_ASEP}}{L_{P\_Lurban}} \sim \frac{a_{wot\_ASEP}}{a_{urban}}$$

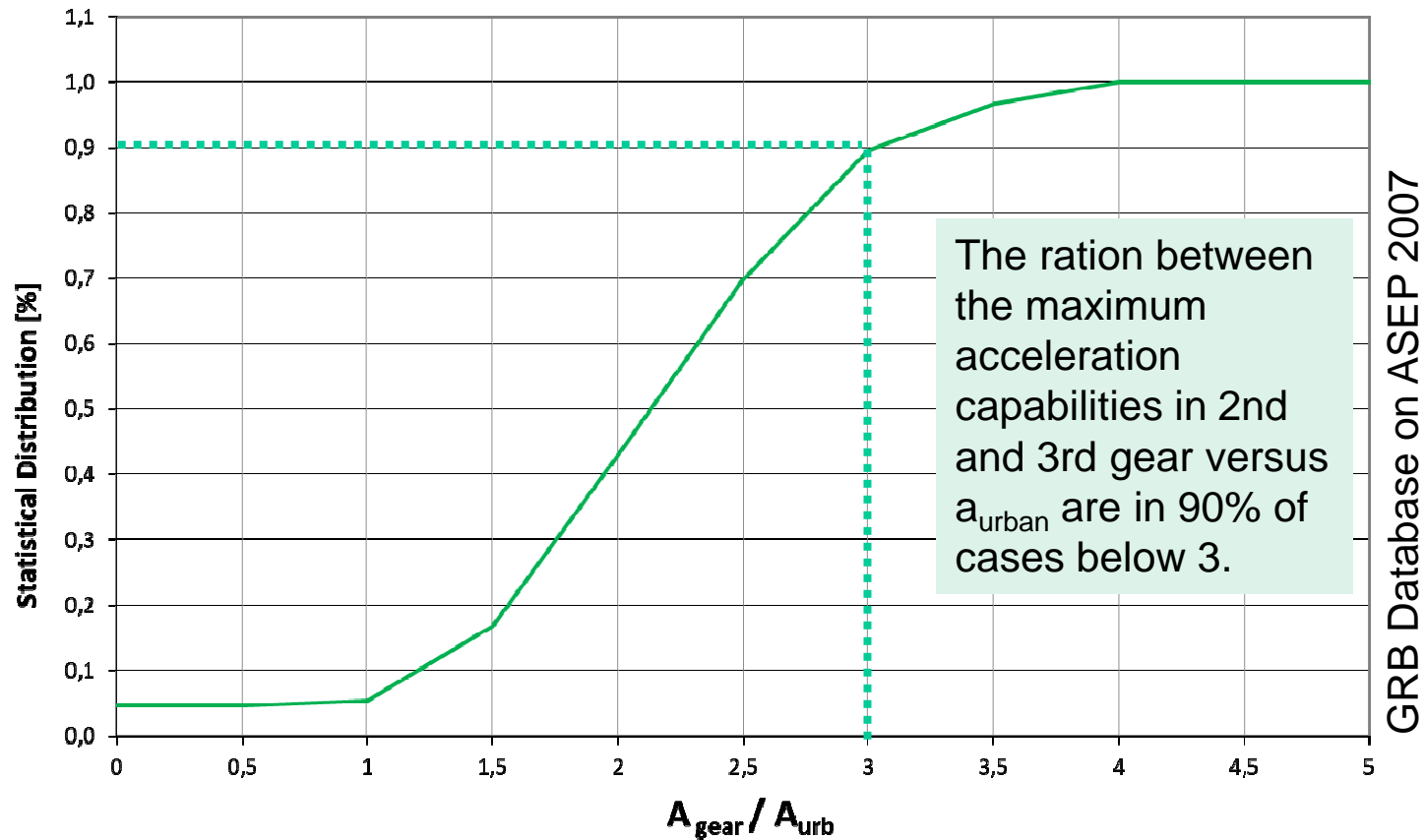
A  $\Delta L_{ASEP}$  of 6 decibel is quoted by the acceleration ratio between the achieved acceleration and  $a_{urban}$ .

## ***Acceleration Potential per Gear***

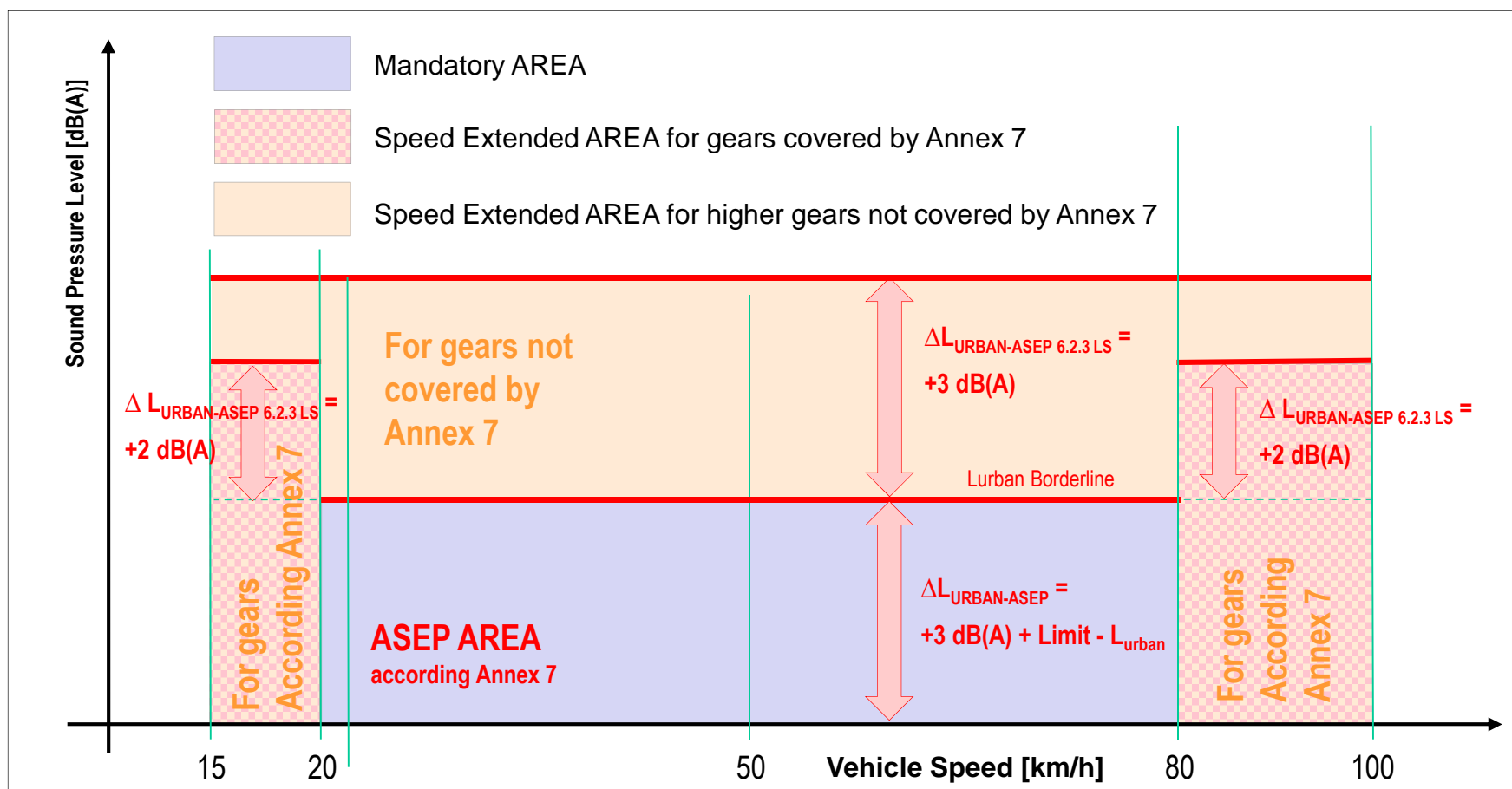
- The acceleration is gear dependant.
- Low gears provide high acceleration potentials at low speeds, while high gears provide limited acceleration potential at higher speeds.
- The IWG ASEP suggests 2 dB for the gears covered by the ASEP control range Annex 7 paragraph 2.5, and 3 dB for any other gears.
- The gears included in the ASEP control range are lower gears with higher acceleration capabilities, mostly 2<sup>nd</sup> and 3<sup>rd</sup> gear.
  - When making a rating between the acceleration potential in these low gears versus the applicable urban, the ratio is mostly not exceeding the factor 3.
  - That means a  $\Delta L_{ASEP}$  of 6 dB would be quoted with 2 dB.
- All other gears – higher gears - will have much less acceleration performance. The ratio would be much lower than the factor 3. In lack of data, a factor 2 is estimated.
  - For these gears a  $\Delta L_{ASEP}$  of 6 dB would be quoted with 3 dB.

## Acceleration Potential in Low Gears

Ratio Between Acceleration Potential In 2nd & 3rd Gear versus Urban Acceleration



## Limitation Concept for $L_{urban}$ Assessment







# **Sound Prediction Model**

## **Correction to the Model**

## Clarification on $\Delta L_{DYN}$ Calculation

$$\Delta L_{DYN} = WENN(E16-E17 < 1; 0; 10 * \log \left( \underbrace{10^{E16/10}}_{L_{WOT,REP}} - \underbrace{10^{((E23 * \log(E14/50) + E22)/10)}}_{L_{TR@VBB,WOT,REP}} - \underbrace{10^{((E29 * \log((E13+E31)/(E27+E31)) + E28)/10)}}_{L_{PT@NBB,WOT,REP}} \right) - \underbrace{E35}_{L_{DYN,REF,NL}})$$

To be deleted

Two times dynamic load considered ???

- The formula shall calculate the delta dynamic between no load and full load.
- Within the energetic calculation the  $L_{DYN,REF,NL}$  is incorrectly considered and shall be deleted.
- There is little impact of this mistake, as  $L_{DYN,REF,NL}$  is always low, mostly 15 dB or more below the energy of tyre rolling sound and meachanical sound.

E16 = Lwot,rep

E14 = vBB,WOT,REP

E13 = NBB,WOT,REP

E28 = LREF,PT,NL

E17 = Lcrs, rep

E22 = LREF,TR

E31 = NSHIFT,PT,NL

E35 = LREF,DYN,NL

E23 = Slopecrs,<50km/h

E29 = Slope,PT,<NBB,CRS,REP

E27 = NBB,CRS,REP