

ASEP IWG #12

2019.07.09-11

ASEP IWG #12 meeting

@Berlin

JASIC

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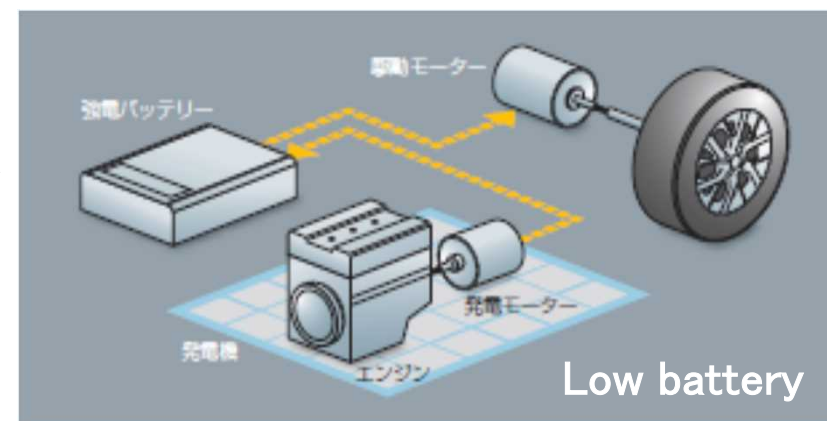
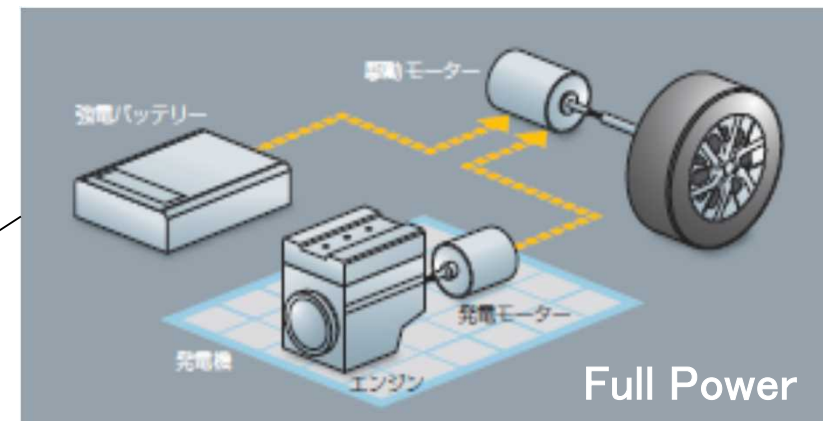
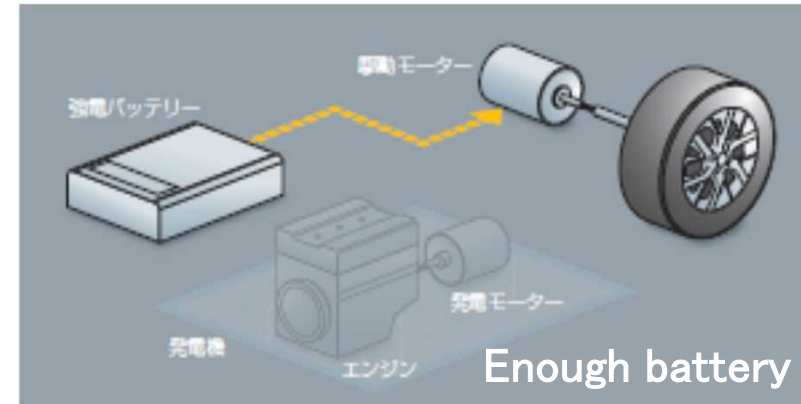
1. ASEP Sound Model - Apply to Series-HEV

Mechanism of Series HEV

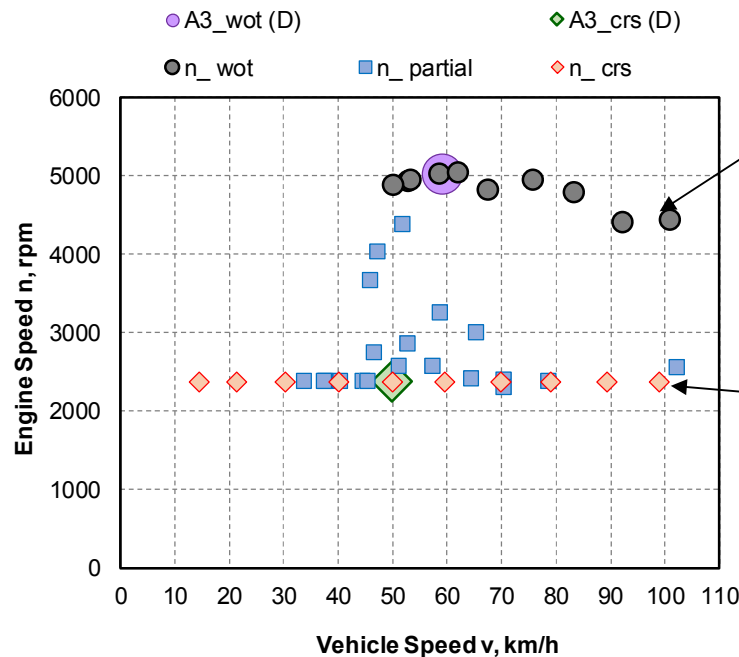
Driven by motor

ICE is only as generator.

No relationship between vehicle speed and ICE engine speed.



Series-HEV



Test vehicle information

Test vehicle		Vehicle-08 (Series-HEV)		
Spec.	Category	M1		
	Power unit	Motor		
	Max. power	80 kW		
	mro	1285 kg		
	PMR	62.3		
	Engine for power generation	1198 cc		
	Tyre size	185/70R14		
R51-03 Annex 3		D-range		
Conditions	Gear	V, km/h	n, rpm	a, m/s ²
Vehicle running (Wot, Partial, Crs)	D	14-103	2400-5000	0.3-4.0



Overview of Sound Model

A Tyre Rolling Sound Model, L_{TR}

$$L_{TR} = \text{Slope}_{TR} * \log(v_{\text{test}} / 50) + L_{REF,TR}$$

$$L_{REF,TR} = X \% \text{ of } L_{CRS,REP}$$

X % (Tyre noise contribution at cruise test in Annex 3 is actually set to by 90%)

B Power Train Base Mechanic Sound Model (No Load), $L_{PT,NL}$

$$L_{PT,NL} = \text{Slope}_{PT,NL} * \log((n_{\text{test}} + n_{\text{shift}}) / (n_{CRS,REP} + n_{\text{shift}})) + L_{REF,PT,NL}$$

$$L_{REF,PT,NL} = (100 - X \%) \text{ of } L_{CRS,REP}$$

C Dynamic Model, L_{DYN}

$$L_{DYN} = \text{Slope}_{DYN,NL} * \log((n_{\text{test}} + n_{\text{shift}}) / (n_{WOT,REP} + n_{\text{shift}})) + L_{REF,DYN,NL} + \Delta L_{DYN} * \Delta L_{\text{Partial}}$$

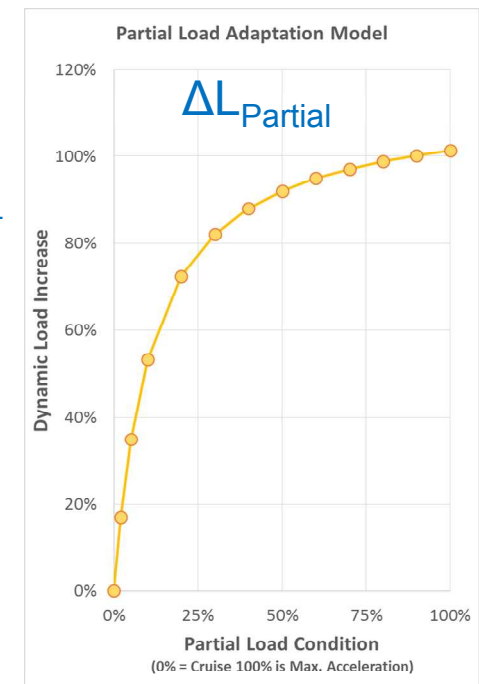
$$L_{REF,DYN,NL} = L_{REF,PT,NL} - 15$$

$$\Delta L_{DYN} = [L_{WOT,REP} \ominus L_{TR}(V_{WOT,REP}) \ominus L_{PT,NL}(n_{WOT,REP})] - L_{REF,DYN,NL}$$

$\Delta L_{\text{Partial}}$ (See right figure)

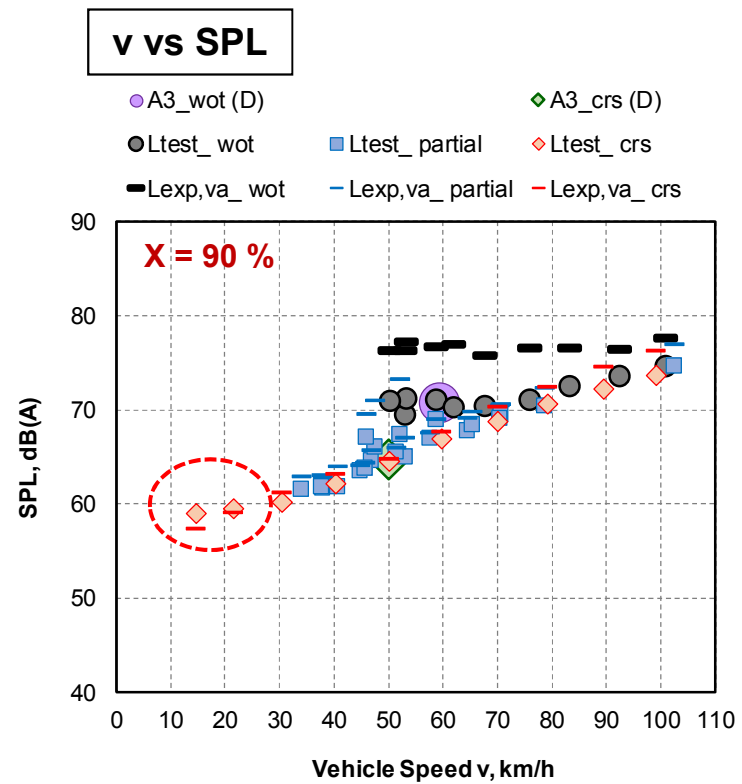
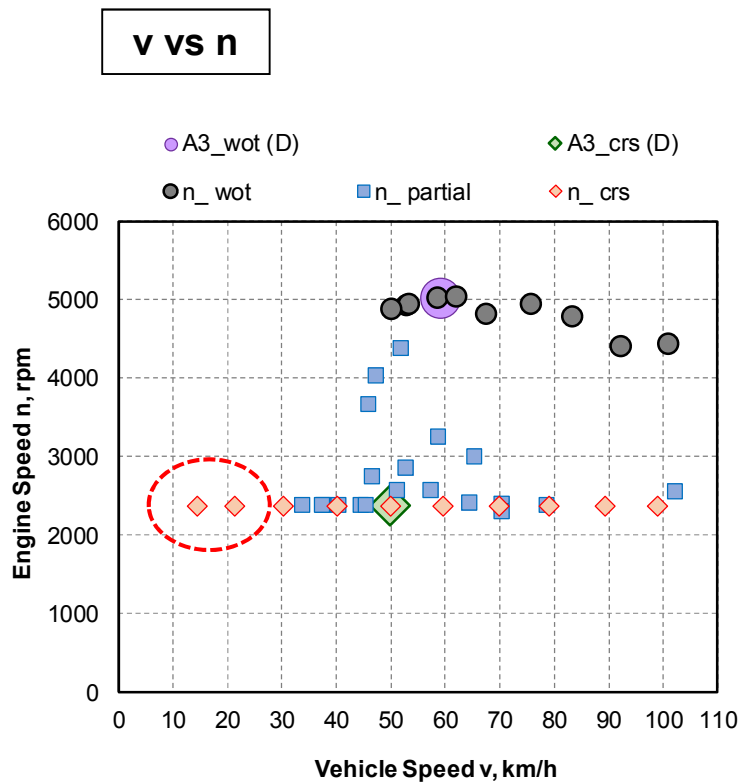
D Expectation level, L_{exp}

$$L_{\text{test}} \leq L_{\text{exp}} = (\underset{\text{A}}{L_{TR}} \oplus \underset{\text{B}}{L_{PT,NL}} \oplus \underset{\text{C}}{L_{DYN}}) + \Delta L_{\text{MARGIN}}$$



An Issue of current sound model

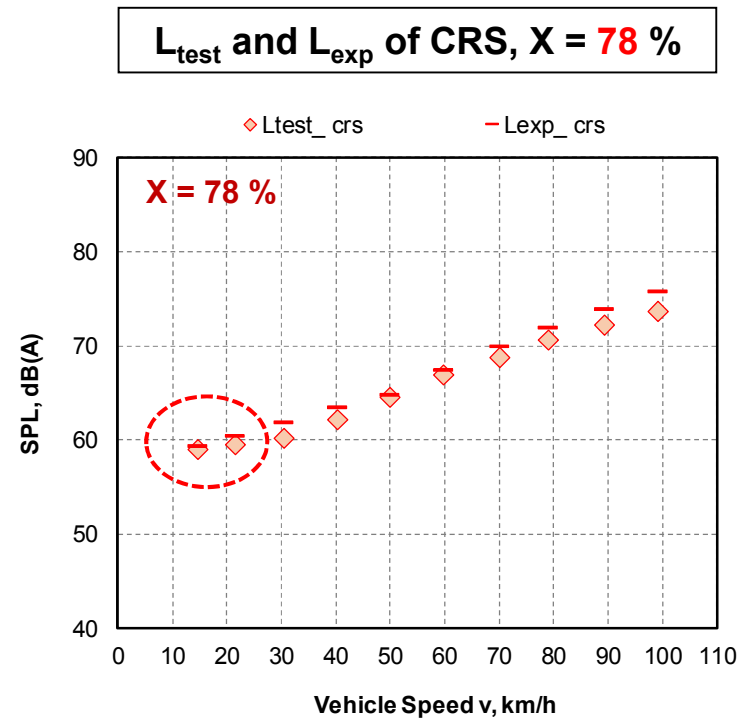
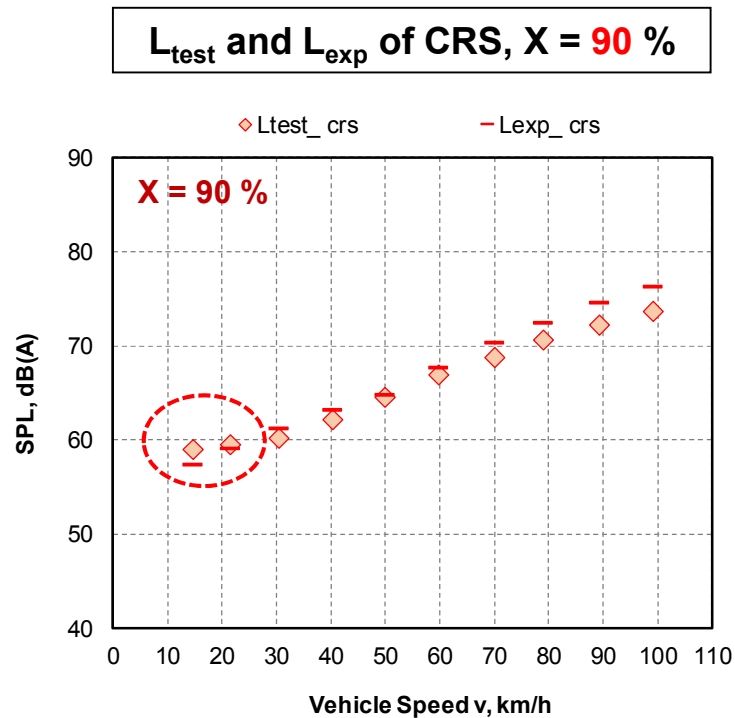
**ASEP sound model can work well at most of conditions.
 Only L_{test} on cruise test at lower vehicle speed exceeds L_{exp}
 by sound model if using $X=90\%$.**



Influence of X(%); tyre noise contribution of L_{crs}

If using **the fixed value $X = 90\%$** ,
 $L_{test} > L_{exp}$ at low vehicle speed.

If using **actual measured value $X=78\%$** , sound model can fit.



The Reason of Underestimation with fixed X=90%

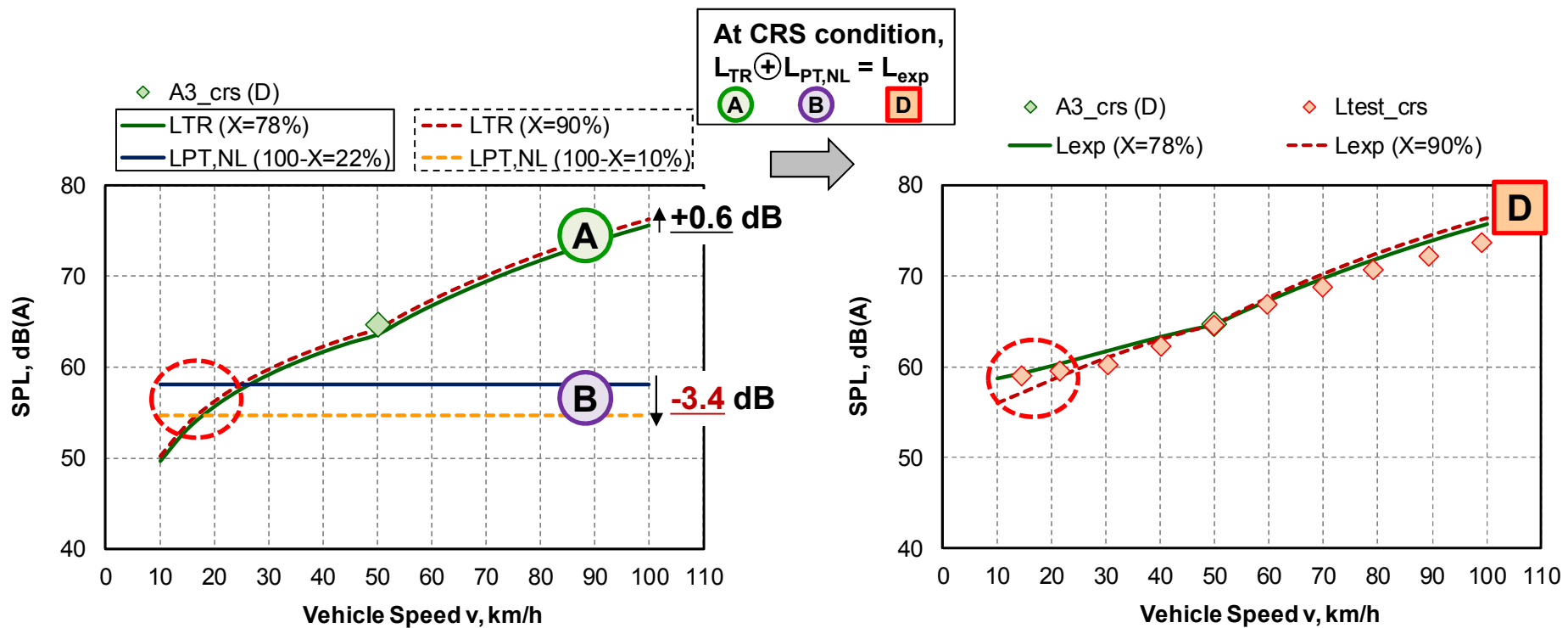
If 78% of X change to 90%,

- (A)** Tyre sound level L_{TR} → +0.6 dB
- (B)** Power train sound level $L_{PT,NL}$ → -3.4 dB

In case of X=90%, $L_{PT,NL}$ (mechanical sound) is underestimated.

Due to higher contribution of $L_{PT,NL}$ at low vehicle speed, L_{exp} is lower than L_{test} .

At higher vehicle speed or acceleration conditions, L_{TR} (tyre sound) and L_{DYN} (dynamic sound) are combined, then less influence of X values.

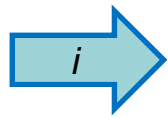


2. Summary of Results

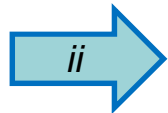
- The sound model can be applied to series HEV at most of operation conditions except for the condition at low speed and low load.
 - In this condition, since mechanical sound model is dominant, estimated uncertainty is not better than the other conditions which sound model is combined three models.
 - Then, X% which links to mechanical sound level is sensitive.
- Need consideration only at low speed and low load condition.

3. Ideas to solve the issue

Using proper value of X for each test car instead of fixed value can improve sound model.



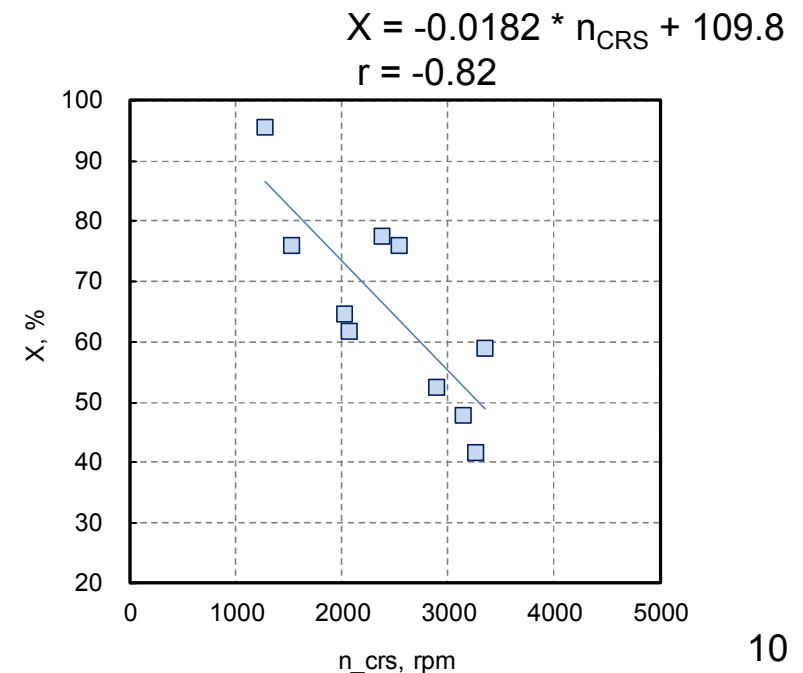
**Measure coast-by test (tyre sound level) to use measured X%
Con; Need additional measurement**



Use formula for relationship between engine speed n_{CRS} and X%.

Function of n_{CRS}
(engine speed in Annex3 cruise test at 50km/h)

$$X (\%) = \frac{10^{\frac{L_{TR}}{10}}}{10^{\frac{L_{CRS}}{10}}} \times 100 = \left(1 - \frac{10^{\frac{L_{pT,NL}}{10}}}{10^{\frac{L_{CRS}}{10}}}\right) \times 100$$



Thank you for your attention.